



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions).

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Fluoranthene		
Target Concentration (C _T)	0.004	mg/l	Origin of C _T : DWS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

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It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Variable	Value	Unit	Source
Contaminant	Fluoranthene		from Level 1
Target Concentration	4.00E-03	mg/l	from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived v)

Variable	Value	Unit	Source
Initial contaminant concentration in groundwater at plume core	1.10E-02	mg/l	See justification table
Half life for degradation of contaminant in water	5.00E+03	days	See justification table
Calculated decay rate	1.39E-04	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	5.50E+02	m	See justification table
Plume thickness at source	2.50E+01	m	See justification table
Saturated aquifer thickness	3.00E+01	m	See justification table
Bulk density of aquifer materials	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	1.00E-01	fraction	See justification table
Hydraulic gradient	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	4.77E+00	m/d	See justification table
Distance to compliance point	1.37E+03	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	0.00E+00	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	0.00E+00	m	See justification table
Time since pollutant entered groundwater	1.00E+100	days	time variant options only
Parameters values determined from options			
Partition coefficient	1.12E+04	l/kg	see options
Longitudinal dispersivity	1.37E+02	m	see options
Transverse dispersivity	1.37E+01	m	see options
Vertical dispersivity	1.37E+00	m	see options

Calculated Parameters

Variable	Value	Unit
Groundwater flow velocity	5.72E-01	m/d
Retardation factor	2.43E+05	fraction
Decay rate used	1.39E-04	d ⁻¹
Rate of contaminant flow due to retardation	2.35E-06	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	0.00E+00	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	breakthrough at compliance point

Remedial Targets

Remedial Target	No impact	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	1373	m	
Concentration of contaminant at compliance point	0.00E+00	mg/l	Ogata Banks
after	1.0E+100	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

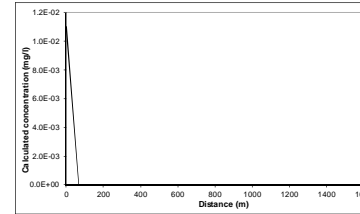
Entry if specify partition coefficient (option)	Kd	l/kg
Soil water partition coefficient		
Entry for non-polar organic chemicals (option)	foc	fraction
Fraction of organic carbon in aquifer	6.16E-01	
Organic carbon partition coefficient	Koc	l/kg
Entry for ionic organic chemicals (option)		
Sorption coefficient for related species	K _{oc,n}	l/kg
Sorption coefficient for ionised species	K _{oc,i}	l/kg
pH value	pH	
acid dissociation constant	pKa	
Fraction of organic carbon in aquifer	foc	fraction
Soil water partition coefficient	Kd	1.12E+04 l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Enter value	Calc value Xu & Eckstein	m
ax	9.70E+00	1.37E+02
ay	0.00E+00	1.37E+01
ay	0.00E+00	1.37E+00

Note values of dispersivity must be > 0
For calculated value, assumes ax = 0.1 * x, az = 0.01 * x, ay = 0.001 * x
Xu & Eckstein (1995) report ax = 0.83(log₁₀x)^{2.414}; az = ax/10, ay = ax/100 are assumed



Calculated concentrations for distance-concentration graph

Ogata Banks	From calculation sheet
Distance	Concentration
	mg/l
0	1.1E-02
68.7	3.85E-22
137.3	1.25E-41
206.0	4.14E-61
274.6	1.40E-80
343.3	4.82E-100
411.9	1.68E-119
480.6	5.87E-139
549.2	2.07E-158
617.9	7.31E-178
686.5	2.60E-197
755.2	9.25E-217
823.8	3.30E-236
892.5	1.18E-255
961.1	4.25E-275
1029.8	1.53E-294
1098.4	0.00E+00
1167.1	0.00E+00
1235.7	0.00E+00
1304.4	0.00E+00
1373.0	0.00E+00

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included; the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action. Note if contaminant is not subject to first order degradation, then set half life as 9.0E+99.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed:	M64 M6 Link Road
Completed by:	Gabriella Barnes
Date:	#####
Version:	1



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

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<u>Details to be completed for each assessment</u>			
Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Indeno(1,2,3-c,d)pyrene		
Target Concentration (C_T)	0.0001	mg/l	Origin of C_T: DWS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

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R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Variable	Value	Unit	Source
Contaminant	Indeno(1,2,3-c,d)pyrene		from Level 1
Target Concentration	1.00E-04	mg/l	from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived v)

Variable	Value	Unit	Source
Initial contaminant concentration in groundwater at plume core	1.28E-02	mg/l	See justification table
Half life for degradation of contaminant in water	1.00E+04	days	See justification table
Calculated decay rate	6.93E-05	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	5.50E+02	m	See justification table
Plume thickness at source	2.50E+01	m	See justification table
Saturated aquifer thickness	3.00E+01	m	See justification table
Bulk density of aquifer materials	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	1.00E-01	fraction	See justification table
Hydraulic gradient	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	4.77E+00	m/d	See justification table
Distance to compliance point	1.37E+03	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	m	See justification table
Time since pollutant entered groundwater	1.00E+100	days	time variant options only
Parameters values determined from options			
Partition coefficient	Kd	l/kg	see options
Longitudinal dispersivity	ax	m	see options
Transverse dispersivity	az	m	see options
Vertical dispersivity	ay	m	see options

Calculated Parameters

Variable	Value	Unit
Groundwater flow velocity	v	5.72E-01 m/d
Retardation factor	Rf	1.16E+06 fraction
Decay rate used	λ	6.93E-05 d ⁻¹
Rate of contaminant flow due to retardation	u	4.92E-07 m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{ED}	0.00E+00 mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	breakthrough at compliance point

Remedial Targets

Remedial Target	No impact	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	1373	m	
Concentration of contaminant at compliance point	C _{ED} /C ₉	0.00E+00 mg/l	Ogata Banks
after		1.0E+100 days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

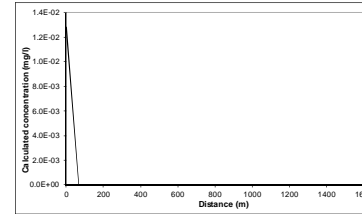
Entry if specify partition coefficient (option)	Kd	l/kg
Soil water partition coefficient	Kd	5.37E+04 l/kg
Entry for non-polar organic chemicals (option)	foc	6.16E-01 fraction
Fraction of organic carbon in aquifer	foc	8.71E+04 l/kg
Organic carbon partition coefficient	Koc	l/kg
Entry for ionic organic chemicals (option)	K _{oc,0}	l/kg
Sorption coefficient for related species	K _{oc,0}	l/kg
Sorption coefficient for ionised species	K _{oc,i}	l/kg
pH value	pH	
acid dissociation constant	pKa	
Fraction of organic carbon in aquifer	foc	fraction

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Enter value	Calc value Xu & Eckstein	m
ax	9.70E+00	1.37E+02
az	0.00E+00	1.37E+01
ay	0.00E+00	1.37E+00

Note values of dispersivity must be > 0
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Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

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This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed:	M4 M6 Link Road
Completed by:	Gabriella Barnes
Date:	#####
Version:	1

Calculated concentrations for distance-concentration graph

Ogata Banks	From calculation sheet
Distance	Concentration
	mg/l
0	1.3E-02
68.7	9.33E-33
137.3	6.28E-63
206.0	4.33E-93
274.6	3.05E-123
343.3	2.18E-153
411.9	1.58E-183
480.6	1.15E-213
549.2	8.40E-244
617.9	6.18E-274
686.5	4.56E-304
755.2	0.00E+00
823.8	0.00E+00
892.5	0.00E+00
961.1	0.00E+00
1029.8	0.00E+00
1098.4	0.00E+00
1167.1	0.00E+00
1235.7	0.00E+00
1304.4	0.00E+00
1373.0	0.00E+00



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Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Naphthalene		
Target Concentration (C_T)	0.006	mg/l	Origin of C_T: DWS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

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R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant **Naphthalene**
Target Concentration **C_t** **6.00E-03** mg/l

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks Equations in HRA publication

Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	9.30E-03	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	1.00E+03	days	See justification table
Calculated decay rate	λ	6.93E-04	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	8.00E+02	m	See justification table
Plume thickness at source	Sy	2.00E+01	m	See justification table
Saturated aquifer thickness	ds	3.00E+01	m	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E+00	m/d	See justification table
Distance to compliance point	x	1.37E+03	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	0.00E+00	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	m	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only
Parameters values determined from options				
Partition coefficient	Kd	3.98E+02	kg	see options
Longitudinal dispersivity	ax	1.37E+02	m	see options
Transverse dispersivity	az	1.37E+01	m	see options
Vertical dispersivity	ay	1.37E+00	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-01	m/d
Retardation factor	Rf	8.63E+03	fraction
Decay rate used	λ	6.93E-04	d ⁻¹
Rate of contaminant flow due to retardation	U	6.63E-05	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{up}	1.17E+165	mg/l
Attenuation factor (one way vertical dispersion, COCED)	AF	7.94E+162	

Remedial Targets

Remedial Target	4.76E+160	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	1373	m	
Concentration of contaminant at compliance point after	C _{up} /C ₀	1.17E+165	mg/l
		1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

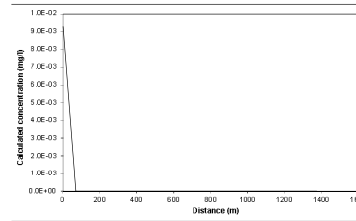
Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)	Kd	3.98E+02	kg
Soil water partition coefficient			
Entry for non-polar organic chemicals (option)	foc	6.16E-01	fraction
Fraction of organic carbon in aquifer			
Organic carbon partition coefficient	Koc	6.46E+02	kg
Entry for ionic organic chemicals (option)			
Sorption coefficient for related species	K _{oc,n}	3.98E+02	kg
Sorption coefficient for ionised species	K _{oc,i}	3.98E+02	kg
pH value	pH	7.00E+00	
Acid dissociation constant	pKa	7.00E+00	
Fraction of organic carbon in aquifer	foc	6.16E-01	fraction
Soil water partition coefficient	Kd	3.98E+02	kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	ax	Enter value	Calc value	Xu & Eckstein	m
Transverse dispersivity	az	0.00E+00	1.37E+01	1.31E+01	m
Vertical dispersivity	ay	0.00E+00	1.37E+00	1.31E-01	m
Note values of dispersivity must be > 0					
For calculated value, assumes ax = 0.1 * x, az = 0.01 * x, ay = 0.001 * x					
Xu & Eckstein (1995) report ax = 0.85(log ₁₀ x) ^{0.44} , az = ax/10, ay = ax/100 are assumed					



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

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Completed by:	Gabriela Barnes
Date:	02/12/2019
Version:	1

Calculated concentrations for distance-concentration graph

Ogata Banks		
From calculation sheet		
Distance	Concentration	mg/l
0	9.3E-03	
68.7	6.68E-11	
137.3	4.31E-19	
206.0	2.88E-27	
274.6	1.39E-35	
343.3	1.38E-43	
411.9	9.74E-52	
480.6	6.93E-60	
549.2	4.97E-68	
617.9	3.69E-76	
686.5	2.80E-84	
755.2	1.89E-92	
823.8	1.38E-100	
892.5	1.01E-108	
961.1	7.37E-117	
1029.8	5.41E-125	
1098.4	3.97E-133	
1167.1	2.92E-141	
1235.7	2.15E-149	
1304.4	1.58E-157	
1373.0	1.17E-165	



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Liability: The Environment Agency does not promise that the worksheet will provide any particular facilities or functions. You must ensure that the worksheet meets your needs and you remain solely responsible for the competent use of the worksheet. You are entirely responsible for the consequences of any use of the worksheet and the Agency provides no warranty about the fitness for purpose or performance of any part of the worksheet. We do not promise that the media will always be free from defects, computer viruses, software locks or other similar code or that the operation of the worksheet will be uninterrupted or error free. You should carry out all necessary virus checks prior to installing on your computing system.

IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions).

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Nickel		
Target Concentration (C _T)	0.02	mg/l	Origin of C _T : DWS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

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Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Nickel	from Level 1
Target Concentration	$2.00E-02$	from Level 1
C_T		

Ogata Banks

Simulate vertical dispersion in 1 direction

Approach for simulating vertical dispersion:

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived v)

Initial contaminant concentration in groundwater at plume core	C_0	$2.32E-02$	mg/l	Source of parameter value
Half life for degradation of contaminant in water	$t_{1/2}$	$1.00E+09$	days	See justification table
Calculated decay rate	λ	$6.93E-10$	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	$8.00E+02$	m	See justification table
Plume thickness at source	Sy	$2.50E+01$	m	See justification table
Saturated aquifer thickness	da	$3.00E+01$	m	See justification table
Bulk density of aquifer materials	ρ	$2.17E+00$	g/cm ³	See justification table
Effective porosity of aquifer	n	$1.00E-01$	fraction	See justification table
Hydraulic gradient	i	$1.20E-02$	fraction	See justification table
Hydraulic conductivity of aquifer	K	$4.77E+00$	m/d	See justification table
Distance to compliance point	x	$1.37E+03$	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	$0.00E+00$	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	$0.00E+00$	m	See justification table
Time since pollutant entered groundwater	t	$1.00E+100$	days	time variant options only
Parameters values determined from options				
Partition coefficient	Kd	$2.00E+03$	l/kg	see options
Longitudinal dispersivity	ax	$1.37E+02$	m	see options
Transverse dispersivity	az	$1.37E+01$	m	see options
Vertical dispersivity	ay	$1.37E+00$	m	see options

Calculated Parameters

Groundwater flow velocity	v	$5.72E-01$	m/d
Retardation factor	Rf	$4.34E+04$	fraction
Decay rate used	λ	$6.93E-10$	d ⁻¹
Rate of contaminant flow due to retardation	u	$1.32E-05$	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C_{ED}	$6.56E-03$	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	$3.54E+00$	

Remedial Targets

Remedial Target	$7.08E-02$	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	1373	m	
Concentration of contaminant at compliance point	$6.56E-03$	mg/l	Ogata Banks
after	$1.0E+100$	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is $9.9E+99$.

Select Method for deriving Partition Co-efficient (using pull down menu)

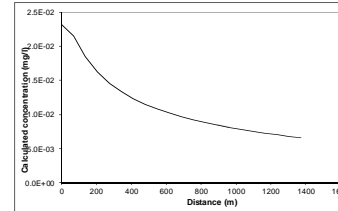
User specified value for partition coefficient

Entry if specify partition coefficient (option)	Kd	$2.00E+03$	l/kg
Soil water partition coefficient	Kd		
Entry for non-polar organic chemicals (option)	foc		fraction
Fraction of organic carbon in aquifer	foc		
Organic carbon partition coefficient	Koc		l/kg
Entry for ionic organic chemicals (option)	K _{oc,ion}		l/kg
Sorption coefficient for related species	K _{oc,ion}		
Sorption coefficient for ionised species	K _{oc,ion}		l/kg
pH value	pH		
acid dissociation constant	pKa		
Fraction of organic carbon in aquifer	foc		fraction
Soil water partition coefficient	Kd	$2.00E+03$	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

	Enter value	Calc value Xu & Eckstein
Longitudinal dispersivity	ax	0.00E+00 1.37E+02 1.37E+01
Transverse dispersivity	az	0.00E+00 1.37E+01 1.37E+00
Vertical dispersivity	ay	0.00E+00 1.37E+00 1.37E+00
Note values of dispersivity must be > 0		
For calculated value, assumes ax = 0.1 * x, az = 0.01 * x, ay = 0.001 * x		
Xu & Eckstein (1995) report ax = 0.83(log ₁₀ x) ^{2.414} ; ax = ax/10, ay = ax/100 are assumed		



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included; the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action. Note if contaminant is not subject to first order degradation, then set half life as $9.0E+99$.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed: M4 M6 Link Road

Completed by: Gabriela Barnes

Date: #####

Version: 1

Calculated concentrations for distance-concentration graph

Ogata Banks
From calculation sheet
Distance Concentration

	mg/l
0	$2.3E-02$
68.7	$2.15E-02$
137.3	$1.85E-02$
206.0	$1.62E-02$
274.6	$1.46E-02$
343.3	$1.33E-02$
411.9	$1.23E-02$
480.6	$1.15E-02$
549.2	$1.08E-02$
617.9	$1.02E-02$
686.5	$9.71E-03$
755.2	$9.25E-03$
823.8	$8.84E-03$
892.5	$8.47E-03$
961.1	$8.13E-03$
1029.8	$7.82E-03$
1098.4	$7.53E-03$
1167.1	$7.26E-03$
1235.7	$7.01E-03$
1304.4	$6.78E-03$
1373.0	$6.56E-03$



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions).

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Phenanthrene		
Target Concentration (C _T)	0.004	mg/l	Origin of C _T : DWS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

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Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Phenanthrene	from Level 1
Target Concentration	C _T 4.00E-03	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks Equations in HRA publication

Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	8.39E-03	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	2.50E+02	days	See justification table
Calculated decay rate	λ	2.77E-04	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.50E+02	m	See justification table
Plume thickness at source	Sy	2.50E+01	m	See justification table
Saturated aquifer thickness	da	3.00E+01	m	See justification table
Bulk density of aquifer materials	p	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E+00	m/d	See justification table
Distance to compliance point	x	1.37E+03	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	0.00E+00	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	m	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options

Partition coefficient	Kd	3.39E+03	l/kg	see options
Longitudinal dispersivity	α _L	1.37E+02	m	see options
Transverse dispersivity	α _T	1.37E+01	m	see options
Vertical dispersivity	α _V	1.37E+00	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-01	m/d
Retardation factor	Rf	7.35E+04	fraction
Decay rate used	λ	2.77E-04	d ⁻¹
Rate of contaminant flow due to retardation	u	7.79E-06	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{0D}	8.51E-305	mg/l
Attenuation factor (one way vertical dispersion, COCED)	AF	8.84E+301	

Remedial Targets

Remedial Target	3.94E+299	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	1373	m	
Concentration of contaminant at compliance point after	C _{0D} /C ₀	8.51E-305	mg/l Ogata Banks
		1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)

Soil water partition coefficient

Entry for non-polar organic chemicals (option)

Fraction of organic carbon in aquifer

Organic carbon partition coefficient

Entry for ionic organic chemicals (option)

Sorption coefficient for related species

Sorption coefficient for ionised species

pH value

acid dissociation constant

Fraction of organic carbon in aquifer

Soil water partition coefficient

K_d 3.39E+03 l/kgf_{oc} 6.16E-01 fractionK_{oc} 5.50E+03 l/kgK_{ocn} 1.00E+00 l/kgK_{ocv} 1.00E+00 l/kg

pH 1.00E+00

pK_a 1.00E+00f_{oc} 1.00E+00 fractionK_d 3.39E+03 l/kg

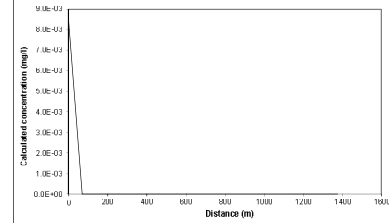
Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	α _L	Enter value	Calc. value	Xu & Eckstein	m
Transverse dispersivity	α _T	1.37E+02	1.37E+01	1.31E+00	m
Vertical dispersivity	α _V	1.37E+00	1.37E+00	1.31E+00	m

Note values of dispersivity must be > 0

For calculated value, assumes α_L = 0.1 * x, α_T = 0.01 * x, α_V = 0.001 * x
Xu & Eckstein (1995) report α_L = 0.83(log₁₀x)^{2.414}, α_T = α_L/10, α_V = α_L/100 are assumed



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included; the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+99.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed	M54 M6 Link Road
Completed by	Gabriella Barnes
Date	09/12/2018
Version	1

Calculated concentrations for distance-concentration graph

Ogata Banks		
From calculation sheet		
Distance	Concentration	
		mg/l
0	8.4E-03	
88.7	6.63E-18	
137.3	4.85E-33	
206.0	3.63E-48	
274.6	2.77E-63	
343.3	2.15E-78	
411.9	1.69E-93	
480.6	1.34E-108	
549.2	1.06E-123	
617.9	8.48E-139	
686.5	6.80E-154	
755.2	5.47E-169	
823.8	4.41E-184	
892.5	3.57E-199	
961.1	2.89E-214	
1029.8	2.35E-229	
1098.4	1.91E-244	
1167.1	1.56E-259	
1235.7	1.27E-274	
1304.4	1.04E-289	
1373.0	8.51E-305	



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions).

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Pyrene		
Target Concentration (C_T)	0.009	mg/l	Origin of C_T: DWS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

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The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Pyrene	from Level 1
Target Concentration	$9.00\text{E-}03$	from Level 1
C_T		

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks Equations in HRA publication

Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived)

Initial contaminant concentration in groundwater at plume core	C_0	$9.62\text{E-}03$	mg/l	See justification table
Half life for degradation of contaminant in water	$t_{1/2}$	$7.50\text{E+}03$	days	See justification table
Calculated decay rate	λ	$9.24\text{E-}05$	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	$8.00\text{E+}02$	m	See justification table
Plume thickness at source	Sy	$2.50\text{E+}01$	m	See justification table
Saturated aquifer thickness	da	$3.00\text{E+}01$	m	See justification table
Bulk density of aquifer materials	ρ	$2.17\text{E+}00$	g/cm ³	See justification table
Effective porosity of aquifer	n	$1.00\text{E-}01$	fraction	See justification table
Hydraulic gradient	i	$1.20\text{E-}02$	fraction	See justification table
Hydraulic conductivity of aquifer	K	$4.77\text{E+}00$	m/d	See justification table
Distance to compliance point	x	$1.37\text{E+}03$	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	$0.00\text{E+}00$	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	$0.00\text{E+}00$	m	See justification table
Time since pollutant entered groundwater	t	$1.00\text{E+}100$	days	time variant options only
Parameters values determined from options				
Partition coefficient	Kd	$9.98\text{E+}03$	l/kg	see options
Longitudinal dispersivity	ax	$1.37\text{E+}02$	m	see options
Transverse dispersivity	az	$1.37\text{E+}01$	m	see options
Vertical dispersivity	ay	$1.37\text{E+}00$	m	see options

Calculated Parameters Variable

Groundwater flow velocity	v	$5.72\text{E-}01$	m/d
Retardation factor	Rf	$2.17\text{E+}06$	fraction
Decay rate used	λ	$9.24\text{E-}05$	d ⁻¹
Rate of contaminant flow due to retardation	u	$2.64\text{E-}06$	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C_{ED}	$4.95\text{E-}302$	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	$1.94\text{E+}299$	

Remedial Targets

Remedial Target	$1.75\text{E+}297$	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	1373	m	
Concentration of contaminant at compliance point after	C_{ED}/C_0	$4.95\text{E-}302$	mg/l
		$1.0\text{E+}100$	days
			Ogata Banks

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is $9.9\text{E+}99$.

Select Method for deriving Partition Co-efficient (using pull down menu)

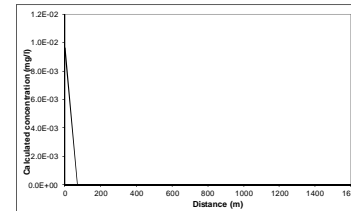
Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)	Kd		l/kg
Soil water partition coefficient			
Entry for non-polar organic chemicals (option)	foc	$6.16\text{E-}01$	fraction
Fraction of organic carbon in aquifer			
Organic carbon partition coefficient	Koc	$1.62\text{E+}04$	l/kg
Entry for ionic organic chemicals (option)			
Sorption coefficient for related species	$K_{oc,i}$		l/kg
Sorption coefficient for ionised species	$K_{oc,i}$		l/kg
pH value	pH		
acid dissociation constant	pKa		
Fraction of organic carbon in aquifer	foc		fraction
Soil water partition coefficient	Kd	$9.98\text{E+}03$	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	ax	Enter value	Calc value	Xu & Eckstein	m
Transverse dispersivity	az	$0.00\text{E+}00$	$1.37\text{E+}01$	$1.31\text{E+}00$	m
Vertical dispersivity	ay	$0.00\text{E+}00$	$1.37\text{E+}00$	$1.31\text{E-}00$	m
Note values of dispersivity must be > 0					
For calculated value, assumes $ax = 0.1 \cdot x$, $az = 0.01 \cdot x$, $ay = 0.001 \cdot x$					
Xu & Eckstein (1995) report $ax = 0.83(\log_{10} x)^{2.414}$; $az = ax/10$, $ay = ax/100$ are assumed					



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as $9.0\text{E+}99$.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed: M64 M6 Link Road
Completed by: Gabriella Barnes
Date: 02/12/2019
Version: 1

Calculated concentrations for distance-concentration graph

Ogata Banks
From calculation sheet
Distance Concentration

	mg/l
0	$9.6\text{E-}03$
68.7	$1.03\text{E-}17$
137.3	$1.02\text{E-}32$
206.0	$1.04\text{E-}47$
274.6	$1.08\text{E-}62$
343.3	$1.14\text{E-}77$
411.9	$1.22\text{E-}92$
480.6	$1.32\text{E-}107$
549.2	$1.43\text{E-}122$
617.9	$1.56\text{E-}137$
686.5	$1.72\text{E-}152$
755.2	$1.89\text{E-}167$
823.8	$2.09\text{E-}182$
892.5	$2.32\text{E-}197$
961.1	$2.57\text{E-}212$
1029.8	$2.86\text{E-}227$
1098.4	$3.18\text{E-}242$
1167.1	$3.55\text{E-}257$
1235.7	$3.96\text{E-}272$
1304.4	$4.43\text{E-}287$
1373.0	$4.95\text{E-}302$



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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The calculation of equations in this worksheet has been independently checked by Entec (UK) Ltd on behalf of the Environment Agency.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions).

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Xylene Total		
Target Concentration (C_T)	0.5	mg/l	Origin of C_T: DWS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.

Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant		Xylene Total		from Level 1
Target Concentration	C _T	5.00E-01	mg/l	from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
-------------	------------------------------

Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C _i	9.10E-02	mg/l	Source of parameter value
Half life for degradation of contaminant in water	t _{1/2}	5.00E+02	days	See justification table
Calculated decay rate	λ	1.39E-03	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	8.00E+02	m	See justification table
Plume thickness at source	Sy	2.50E+01	m	See justification table
Saturated aquifer thickness	da	3.00E+01	m	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E+00	m/d	See justification table
Distance to compliance point	x	1.37E+03	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	0.00E+00	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	m	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only
Parameters values determined from options				
Partition coefficient	Kd	2.79E+02	l/kg	see options
Longitudinal dispersivity	ax	1.37E+02	m	see options
Transverse dispersivity	az	1.37E+01	m	see options
Vertical dispersivity	ay	1.37E+00	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-01	m/d
Retardation factor	Rf	6.06E+03	fraction
Decay rate used	λ	1.39E-03	d ⁻¹
Rate of contaminant flow due to retardation	u	9.44E-05	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{1D}	3.61E-195	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	2.52E+193	

Remedial Targets

Remedial Target	1.26E+193	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	1373	m	
Concentration of contaminant at compliance point after	C _{1D} /C ₀	3.61E-195 1.0E+100	mg/l days
			Ogata Banks

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target.
The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)

Soil water partition coefficient	Kd		l/kg
Entry for non-polar organic chemicals (option)			
Fraction of organic carbon in aquifer	foc	6.16E-01	fraction
Organic carbon partition coefficient	Koc	4.54E+02	l/kg
Entry for ionic organic chemicals (option)			
Sorption coefficient for related species	K _{oc,n}		l/kg
Sorption coefficient for ionised species	K _{oc,i}		l/kg
pH value	pH		
acid dissociation constant	pKa		
Fraction of organic carbon in aquifer	foc		fraction
Soil water partition coefficient	Kd	2.79E+02	l/kg

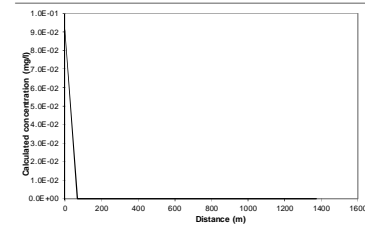
Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	ax	Enter value	Calc value Xu & Eckstein	m
Transverse dispersivity	az	0.00E+00	1.37E+02	1.37E+00
Vertical dispersivity	ay	0.00E+00	1.37E+01	1.37E+00
		0.00E+00	1.37E+00	1.37E-01

Note values of dispersivity must be > 0

For calculated value, assumes ax = 0.1 * x, az = 0.01 * x, ay = 0.001 * x
Xu & Eckstein (1995) report ax = 0.83(log₁₀x)^{2.414}, az = ax/10, ay = ax/100 are assumed



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.
Note if contaminant is not subject to first order degradation, then set half life as 9.0E+99.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Calculated concentrations for distance-concentration graph

Ogata Banks
From calculation sheet

Distance	Concentration
	mg/l
0	9.1E-02
68.7	1.92E-11
137.3	3.76E-21
206.0	7.51E-31
274.6	1.54E-40
343.3	3.20E-50
411.9	6.74E-60
480.6	1.43E-69
549.2	3.07E-79
617.9	6.60E-89
686.5	1.43E-98
755.2	3.09E-108
823.8	6.73E-118
892.5	1.47E-127
961.1	3.21E-137
1029.8	7.03E-147
1098.4	1.54E-156
1167.1	3.38E-166
1235.7	7.44E-176
1304.4	1.64E-185
1373.0	3.61E-195

Site being assessed: M54 M6 Link Road
Completed by: Gabriela Barnes
Date: #####
Version: 1

Simulation Details

Project Number	60536736
Project Title	M54/M6 Link Road
Date	28-Nov-19

Simulation Details	Simulation detailing the potential contaminant concentration in groundwater affecting the surface watercourse Latherford Brook
--------------------	--

LEVEL 3 (GROUNDWATER) ASSESSMENT - INPUTS & JUSTIFICATION

Project Number	60536736
Project Title	M54/M6 Link Road
Date	28-Nov-19

Simulation Details	Simulation detailing the potential contaminant concentration in groundwater affecting the surface watercourse Latherford Brook
--------------------	--

Parameter	Units	Input Value(s)		Source / Justification
Infiltration	mm/year	14.4		Met Office - Based on unsurfaced ground with annual average rainfall of 57.5mm/year
Saturated aquifer thickness	m	30		Assumed thickness of bedrock aquifer
Bulk density of aquifer materials	g/cm ³	2.17		Average Value from geotechnical laboratory analysis over weathered bedrock and bedrock
Effective porosity of aquifer	fraction	0.1		Value for Sandstone from Domenico & Schwartz, 1990
Hydraulic gradient	fraction	0.012		Gradients taken from GW monitoring levels between BH18 and BH27
Hydraulic conductivity of aquifer	m/s	5.52E-06		Average value from geotechnical laboratory analysis
Hydraulic conductivity of aquifer	m/d	4.77E-01		Calculated in m/d
Fraction of Organic Carbon	fraction	0.616		Taken from chemical screening data
Distance to compliance point	m	139		BH21 closest borehole with exceedances south of Latherford Brook
Longitudinal dispersivity	m	13.9		10% of pathway length
Transverse dispersivity	m	1.39		1% of pathway length
Width of plume in aquifer at source	m	550.0	800.0	Width at BH03 and width at BH26 (Areas of maximum concentration)
Plume thickness at source	m	25		Assumed thickness of plume

CONTAMINANT SPECIFIC INPUTS

Project Number	60536736
Project Title	M54/M6 Link Road
Date	28-Nov-19

Simulation Details	Simulation detailing the potential contaminant concentration in groundwater affecting the surface watercourse Latherford Brook
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Determinand	Henry's Law Constant dimensionless	Source	Organic C - water partition coefficient (Koc) l/kg	Source	Soil-Water Partition Coefficient (Kd) l/kg	Source	Background Concentration in Groundwater mg/l	Source	Half-Life of Contaminant in Groundwater days	Source	Initial contaminant concentration in groundwater mg/l	Source
Ethylbenzene (EQS)	1.39E-01	LQM/CIEH 2009, T	4.47E+02	Science Report – SC050021/SR7			0.01	Half of EQS value	5.0E+02	EA: The rationale for t	0.045	Chemical Screening data
Xylene Total (EQS)	1.04E-01	LQM/CIEH 2009, T	4.54E+02	Science Report – SC050021/SR7			0.015	Half of EQS value	5.0E+02	EA: The rationale for t	0.091	Chemical Screening data
Ammoniacal Nitrogen (EQS)					1.0	CONSIM	0.15	Half of EQS value	2.2E+03	EA: The rationale for t	5.46	Chemical Screening data
Naphthalene (EQS)	6.62E-03	Science Report – S	6.46E+02	LQM/CIEH 2009, Temperature corrected to 10oC			0.001	Half of EQS value	1.0E+03	EA: The rationale for t	0.00749	Chemical Screening data
Anthracene (EQS)	1.81E-04	LQM/CIEH 2009, T	5.62E+03	LQM/CIEH 2009, Temperature corrected to 10oC			0.0001	Half of EQS value	3.0E+03	URS/PAHs: The ratio	0.00220	Chemical Screening data
Fluoranthene (EQS)	6.29E-05	Science Report – S	1.82E+04	LQM/CIEH 2009, Temperature corrected to 10oC			3.2E-06	Half of EQS value	5.0E+03	URS/PAHs: The ratio	0.01100	Chemical Screening data
Benzo(a) pyrene (EQS)	1.76E-06	Science Report – S	1.29E+05	LQM/CIEH 2009, Temperature corrected to 10oC			0.000000085	Half of EQS value	1.0E+04	(3) URS/PAHs: The ra	0.0159	Chemical Screening data
Benzo(g,h,i)perylene (EQS)	2.86E-06	LQM/CIEH 2009, T	4.17E+05	LQM/CIEH 2009, Temperature corrected to 10oC			0.00000041	Half of EQS value	1.0E+04	(3) URS/PAHs: The ra	0.004	Chemical Screening data
Benzo(k)fluoranthene (EQS)	2.05E-06	Science Report – S	1.05E+05	LQM/CIEH 2009, Temperature corrected to 10oC			0.00000085	Half of EQS value	1.0E+04	(3) URS/PAHs: The ra	0.02450	Chemical Screening data
Benzo(k)fluoranthene (EQS)	1.74E-06	Science Report – S	1.48E+05	LQM/CIEH 2009, Temperature corrected to 10oC			0.00000085	Half of EQS value	1.0E+04	(3) URS/PAHs: The ra	0.00774	Chemical Screening data
Phenol (EQS)	8.35E-06	Science Report – S	8.32E+01	Science Report – SC050021/SR7			0.00385	Half of EQS value	3.5E+02	EA: The rationale for t	0.08700	Chemical Screening data
Bis(2-ethylhexyl) phthalate (EQS)	5.33E-05	h calc, compensate	8.74E+04	www.toxnet.nlm.nih.gov			0.00065	Half of EQS value	1.0E+04	URS/A&H: The ration	0.12700	Chemical Screening data
Cadmium (EQS)					2560.0	CLEA UK	0.00004	Half of EQS value	1.0E+09	URS CWRA DATABA	0.00461	Chemical Screening data
Chromium (hexavalent) (EQS)					4800.0	CLEA UK	0.0017	Half of EQS value	1.0E+09	URS CWRA DATABA	0.02780	Chemical Screening data
Copper (EQS)					35.0	CLEA UK	5.0E-04	Half of EQS value	1.0E+09	URS CWRA DATABA	0.01240	Chemical Screening data
Nickel (EQS)					2000.0	CLEA UK	0.002	Half of EQS value	1.0E+09	URS CWRA DATABA	0.0232	Chemical Screening data
Zinc (EQS)					36.0	2001, USEPA, Sup	0.00545	Half of EQS value	1.0E+09	URS CWRA DATABA	0.0401	Chemical Screening data



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Ammoniacal Nitrogen		
Target Concentration (C_T)	0.3 mg/l	Origin of C_T :	EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

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It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Ammoniacal Nitrogen	from Level 1
Target Concentration	C _t 3.00E-01	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	5.48E+00	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	2.19E+03	days	See justification table
Calculated decay rate	λ	3.17E-04	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.55E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	x	1.38E+02	rr	See justification table
Distance to compliance point	z	0.00E+00	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options

Partition coefficient	Kd	1.00E+00	l/kg	see options
Longitudinal dispersivity	αx	1.38E+01	m	see options
Transverse dispersivity	αz	1.38E+00	m	see options
Vertical dispersivity	αy	1.38E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d
Retardation factor	Rf	2.27E+01	fraction
Decay rate used	λ	3.17E-04	d ⁻¹
Rate of contaminant flow due to retardation	u	2.52E-03	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	5.95E-04	mg/l
Attenuation factor (one way vertical dispersion, COCED)	AF	9.17E+03	

Remedial Targets

Remedial Target	2.75E+03	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C _{eq} /C ₀ 5.95E-04	mg/l	Ogata Banks
	1.0E+100	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

User specified value for partition coefficient

Entry if specify partition coefficient (option)	Kd	1.00E+00	l/kg
Soil water partition coefficient	Kd	1.00E+00	l/kg
Entry for non-polar organic chemicals (option)	foc	0.00E+00	fraction
Fraction of organic carbon in aquifer	foc	0.00E+00	fraction
Organic carbon partition coefficient	Koc	0.00E+00	l/kg
Entry for ionic organic chemicals (option)	K _{oc,n}	0.00E+00	l/kg
Sorption coefficient for related species	K _{oc,n}	0.00E+00	l/kg
Sorption coefficient for ionised species	pH	0.00E+00	l/kg
pH value	pKa	0.00E+00	fraction
acid dissociation constant	foc	0.00E+00	fraction
Fraction of organic carbon in aquifer	Kd	1.00E+00	l/kg
Soil water partition coefficient	Kd	1.00E+00	l/kg

Define dispersivity (click brown cell and use pull down list)

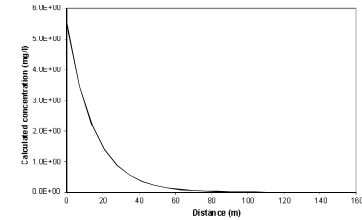
Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	αx	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	αz	0.00E+00	1.38E+01	5.20E+00	m
Vertical dispersivity	αy	0.00E+00	1.38E+00	5.72E-01	rr
Vertical dispersivity	αy	0.00E+00	1.38E-01	5.23E-02	rr

Note values of dispersivity must be > 0

For calculated value, assumes αx = 0.1 * x, αz = 0.01 * x, αy = 0.001 * x

Xu & Eckstein (1995) report αx = 0.83(log₁₀)^{2.44}, αz = αx/10, αy = αx/100 are assumed



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Anthracene		
Target Concentration (C_T)	0.0001	mg/l	Origin of C_T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.

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It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Anthracene	from Level 1
Target Concentration	C _t 1.00E-04	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	2.20E-03	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	3.00E+03	days	See justification table
Calculated decay rate	λ	2.31E-04	days ⁻¹	
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.50E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance to compliance point	x	1.39E+02	rr	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	0.00E+00	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options

Partition coefficient	Kd	3.48E+03	l/kg	see options
Longitudinal dispersivity	αx	1.39E+01	m	see options
Transverse dispersivity	αz	1.39E+00	m	see options
Vertical dispersivity	αy	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d
Retardation factor	Rf	7.52E+04	fraction
Decay rate used	λ	2.31E-04	days ⁻¹
Rate of contaminant flow due to retardation	u	7.61E-07	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	2.88E-283	mg/l
Attenuation factor (one way vertical dispersion, COCED)	AF	7.70E+279	

Remedial Targets

Remedial Target	7.70E+275	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C _{eq} /C ₀ 2.88E-283	mg/l	Ogata Banks
	1.0E+100	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)

Soil water partition coefficient

K_d 3.48E+03 l/kg

Entry for non-polar organic chemicals (option)

Fraction of organic carbon in aquifer

f_{oc} 6.18E-01 fraction

Organic carbon partition coefficient

K_{oc} 5.62E+03 l/kg

Entry for ionic organic chemicals (option)

Sorption coefficient for related species

K_{oc,n} 3.48E+03 l/kg

Sorption coefficient for ionised species

K_{oc,i} 3.48E+03 l/kg

pH value

pH 3.48E+03 l/kg

acid dissociation constant

pKa 3.48E+03 l/kg

Fraction of organic carbon in aquifer

f_{oc} fraction

Soil water partition coefficient

K_d 3.48E+03 l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity

αx Enter value 1.39E+01 Calc value 1.39E+01 Xu & Eckstein rr

Transverse dispersivity

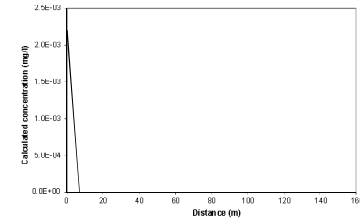
αz Enter value 1.39E+00 Calc value 1.39E+00 rr

Vertical dispersivity

αy Enter value 1.39E-01 Calc value 1.39E-01 rr

Note values of dispersivity must be > 0

For calculated value, assumes αx = 0.1 * x, αz = 0.01 * x, αy = 0.001 * x

Xu & Eckstein (1995) report αx = 0.83(log₁₀)^{2.41H}, αz = αx/10, αy = αx/100 are assumed

Calculated concentrations for distance-concentration graph

Ogata Banks
From calculation sheet

Distance	Concentration
	mg/l
0	2.2E-03
7.0	2.23E-17
13.9	2.26E-31
20.9	2.29E-45
27.8	2.32E-59
34.8	2.35E-73
41.7	2.38E-87
48.7	2.41E-101
55.6	2.44E-115
62.6	2.47E-129
69.5	2.51E-143
76.5	2.54E-157
83.4	2.57E-171
90.4	2.61E-185
97.3	2.64E-199
104.3	2.68E-213
111.2	2.71E-227
118.2	2.75E-241
125.1	2.78E-255
132.1	2.82E-269
139.0	2.86E-283

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Benzo(a)pyrene		
Target Concentration (C_T)	0.00000017	mg/l	Origin of C_T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.

Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note



Input Parameters (using pull down menu)

Contaminant	Benzo(a)pyrene	from Level 1
Target Concentration	C _t 1.70E-07	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	1.59E-02	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	1.00E+04	days	See justification table
Calculated decay rate	λ	6.93E-05	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.59E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	x	1.39E+02	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	z	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options

Partition coefficient	Kd	7.95E+04	l/kg	see options
Longitudinal dispersivity	αx	1.39E+01	m	see options
Transverse dispersivity	αz	1.39E+00	m	see options
Vertical dispersivity	αy	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d	
Retardation factor	Rf	1.72E+06	fraction	
Decay rate used	λ	6.93E-05	days ⁻¹	
Rate of contaminant flow due to retardation	u	3.32E-08	m/d	
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	0.00E+00	mg/l	
Attenuation factor (one way vertical dispersion, COC/ED)	AF	breakthrough at compliance point		

Remedial Targets

Remedial Target	No Impact	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point	C _{eq} /C ₀	0.00E+00	mg/l Ogata Banks
after		1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)

Soil water partition coefficient

K_d 7.95E+04 l/kg

Entry for non-polar organic chemicals (option)

Fraction of organic carbon in aquifer

f_{oc} 6.18E-01 fraction

Organic carbon partition coefficient

K_{oc} 1.29E+05 l/kg

Entry for ionic organic chemicals (option)

Sorption coefficient for related species

K_{oc,n} 7.95E+04 l/kg

Sorption coefficient for ionised species

K_{oc,i} 7.95E+04 l/kg

pH value

pH 7.95E+04 l/kg

acid dissociation constant

pKa 7.95E+04 l/kg

Fraction of organic carbon in aquifer

f_{oc} 6.18E-01 fraction

Soil water partition coefficient

K_d 7.95E+04 l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity

αx 1.39E+01 m

Transverse dispersivity

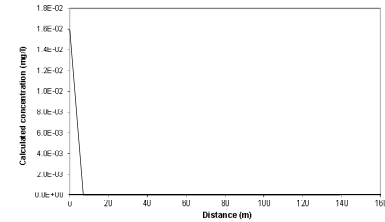
αz 1.39E+00 m

Vertical dispersivity

αy 1.39E-01 m

Note values of dispersivity must be > 0

For calculated value, assumes αx = 0.1 * x, αz = 0.01 * x, αy = 0.001 * x

Xu & Eckstein (1995) report αx = 0.83(log₁₀)^{2.44}, αz = αx/10, αy = αx/100 are assumed

Calculated concentrations for distance-concentration graph

Ogata Banks
From calculation sheet
Distance Concentration

0	1.6E-02
7.0	2.0E-39
13.9	2.6E-76
20.9	3.47E-113
27.8	4.50E-160
34.8	5.84E-187
41.7	7.57E-224
48.7	9.62E-261
55.6	1.27E-297
62.6	0.00E+00
69.5	0.00E+00
76.5	0.00E+00
83.4	0.00E+00
90.4	0.00E+00
97.3	0.00E+00
104.3	0.00E+00
111.2	0.00E+00
118.2	0.00E+00
125.1	0.00E+00
132.1	0.00E+00
139.0	0.00E+00

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name: M54 M6 Link Road

Site Address:

Completed by: Gabriella Barnes

Date: 02-Dec-19

Version: 1

Contaminant Benzo(b)fluoranthene

Target Concentration (C_T) 0.000017 mg/l

Origin of C_T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.

Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note



Input Parameters (using pull down menu)

Contaminant	Benzo(b)fluoranthene	from Level 1
Target Concentration	C _t 1.70E-05	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	2.45E-02	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	1.00E+04	days	See justification table
Calculated decay rate	λ	6.93E-05	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.50E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	x	1.39E+02	rr	See justification table
Distance to compliance point	z	0.00E+00	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options				
Partition coefficient	Kd	6.47E+04	l/kg	see options
Longitudinal dispersivity	αx	1.39E+01	m	see options
Transverse dispersivity	αz	1.39E+00	m	see options
Vertical dispersivity	αy	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d	
Retardation factor	Rf	1.40E+06	fraction	
Decay rate used	λ	6.93E-05	d ⁻¹	
Rate of contaminant flow due to retardation	u	4.08E-08	m/d	
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	0.00E+00	mg/l	
Attenuation factor (one way vertical dispersion, COC/ED)	AF	breakthrough at compliance point		

Remedial Targets

Remedial Target	No impact	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point	C _{eq} /C ₀	0.00E+00	mg/l Ogata Banks
after		1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

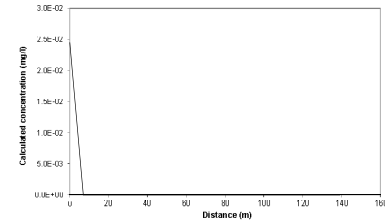
Entry if specify partition coefficient (option)	Kd	6.47E+04	l/kg
Soil water partition coefficient	Kd	6.47E+04	l/kg
Entry for non-polar organic chemicals (option)	foc	6.18E-01	fraction
Fraction of organic carbon in aquifer	foc	6.18E-01	fraction
Organic carbon partition coefficient	Koc	1.05E+05	l/kg
Entry for ionic organic chemicals (option)	Koc,n	6.18E+00	l/kg
Sorption coefficient for related species	Koc,n	6.18E+00	l/kg
Sorption coefficient for ionised species	Koc,n	6.18E+00	l/kg
pH value	pH	6.18E+00	l/kg
acid dissociation constant	pKa	6.18E+00	l/kg
Fraction of organic carbon in aquifer	foc	6.18E-01	fraction
Soil water partition coefficient	Kd	6.47E+04	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	αx	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	αz	0.00E+00	1.39E+01	6.00E+00	m
Vertical dispersivity	αy	0.00E+00	1.39E+00	6.75E-01	rr
Vertical dispersivity	αy	0.00E+00	1.39E-01	6.75E-02	rr

Note values of dispersivity must be > 0
For calculated value, assumes αx = 0.1 * x, αz = 0.01 * x, αy = 0.001 * x
Xu & Eckstein (1995) report αx = 0.83(log₁₀)^{2.44}, αz = αx/10, αy = αx/100 are assumed



Calculated concentrations for distance-concentration graph

Ogata Banks	From calculation sheet
Distance	Concentration
0	2.5E-02
7.0	1.32E-35
13.9	7.11E-69
20.9	3.83E-102
27.8	2.06E-135
34.8	1.11E-168
41.7	5.99E-202
48.7	3.23E-235
55.6	1.74E-268
62.6	9.36E-302
69.5	0.00E+00
76.5	0.00E+00
83.4	0.00E+00
90.4	0.00E+00
97.3	0.00E+00
104.3	0.00E+00
111.2	0.00E+00
118.2	0.00E+00
125.1	0.00E+00
132.1	0.00E+00
139.0	0.00E+00

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name: M54 M6 Link Road

Site Address:

Completed by: Gabriella Barnes

Date: 02-Dec-19

Version: 1

Contaminant Benzo(g,h,i)perylene

Target Concentration (C_T) 0.0000082 mg/l

Origin of C_T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

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Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Benzo(a,h,i)perylene	from Level 1
Target Concentration	C _t 8.20E-06	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	4.00E-03	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	1.00E+04	days	See justification table
Calculated decay rate	λ	8.63E-05	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.50E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance to compliance point	x	1.38E+02	rr	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	1.38E+02	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only
Parameters values determined from options				
Partition coefficient	Kd	2.57E+05	l/kg	see options
Longitudinal dispersivity	αx	1.38E+01	m	see options
Transverse dispersivity	αz	1.38E+00	m	see options
Vertical dispersivity	αy	1.38E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d
Retardation factor	Rf	5.67E+06	fraction
Decay rate used	λ	8.63E-05	d ⁻¹
Rate of contaminant flow due to retardation	u	1.03E-08	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	0.00E+00	mg/l
Attenuation factor (one way vertical dispersion, COC/ED)	AF	breakthrough at compliance point	

Remedial Targets

Remedial Target	No impact	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point	C _{eq} /C ₀	0.00E+00	mg/l Ogata Banks
after		1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)

Soil water partition coefficient	Kd	2.57E+05	l/kg
Entry for non-polar organic chemicals (option)			
Fraction of organic carbon in aquifer	foc	6.18E-01	fraction
Organic carbon partition coefficient	Koc	4.17E+05	l/kg
Entry for ionic organic chemicals (option)			
Sorption coefficient for related species	K _{oc,n}	4.17E+05	l/kg
Sorption coefficient for ionised species	K _{oc,i}	4.17E+05	l/kg
pH value	pH	4.17E+05	l/kg
acid dissociation constant	pKa	4.17E+05	l/kg
Fraction of organic carbon in aquifer	foc	6.18E-01	fraction
Soil water partition coefficient	Kd	2.57E+05	l/kg

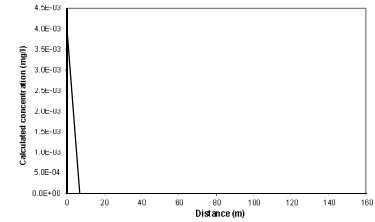
Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	αx	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	αz	0.00E+00	1.38E+01	6.00E+00	m
Vertical dispersivity	αy	0.00E+00	1.38E+00	6.75E-01	rr
Vertical dispersivity	αy	0.00E+00	1.38E-01	6.75E-02	rr

Note values of dispersivity must be > 0

For calculated value, assumes αx = 0.1 * x, αz = 0.01 * x, αy = 0.001 * x
Xu & Eckstein (1995) report αx = 0.83(log₁₀)^{2.41H}, αz = αx/10, αy = αx/100 are assumed



Calculated concentrations for distance-concentration graph

Ogata Banks		
From calculation sheet		
Distance	Concentration	
	mg/l	
0	4.0E-03	
7.0	1.57E-09	
13.9	6.14E-136	
20.9	2.41E-202	
27.8	9.44E-269	
34.8	0.00E+00	
41.7	0.00E+00	
48.7	0.00E+00	
55.6	0.00E+00	
62.6	0.00E+00	
69.5	0.00E+00	
76.5	0.00E+00	
83.4	0.00E+00	
90.4	0.00E+00	
97.3	0.00E+00	
104.3	0.00E+00	
111.2	0.00E+00	
118.2	0.00E+00	
125.1	0.00E+00	
132.1	0.00E+00	
139.0	0.00E+00	

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	02/12/2018
Version	



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Benzo(k)fluoranthene		
Target Concentration (C_T)	0.000017 mg/l	Origin of C_T :	EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.

Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note



Input Parameters (using pull down menu)

Contaminant	Benzo(k)fluoranthene	from Level 1
Target Concentration	C _T 1.70E-05	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	7.14E-03	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	1.00E+04	days	See justification table
Calculated decay rate	λ	6.93E-05	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.50E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	p	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	x	1.39E+02	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	z	0.00E+00	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options

Partition coefficient	Kd	9.12E+04	l/kg	see options
Longitudinal dispersivity	ax	1.39E+01	m	see options
Transverse dispersivity	az	1.39E+00	m	see options
Vertical dispersivity	ay	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d	
Retardation factor	Rf	1.99E+06	fraction	
Decay rate used	λ	6.93E-05	days ⁻¹	
Rate of contaminant flow due to retardation	u	2.89E-08	m/d	
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	0.00E+00	mg/l	
Attenuation factor (one way vertical dispersion, CO/CED)	AF	breakthrough at compliance point		

Remedial Targets

Remedial Target	No Impact	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point	C _{eq} /C ₀	0.00E+00	mg/l Ogata Banks
after		1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)

Soil water partition coefficient	Kd	9.12E+04	l/kg
Entry for non-polar organic chemicals (option)			
Fraction of organic carbon in aquifer	foc	6.18E-01	fraction
Organic carbon partition coefficient	Koc	1.49E+05	l/kg
Entry for ionic organic chemicals (option)			
Sorption coefficient for related species	K _{oc,n}	9.12E+04	l/kg
Sorption coefficient for ionised species	K _{oc,i}	9.12E+04	l/kg
pH value	pH	9.00E+00	l/kg
acid dissociation constant	pKa	9.00E+00	fraction
Fraction of organic carbon in aquifer	foc	9.12E+04	l/kg
Soil water partition coefficient	Kd	9.12E+04	l/kg

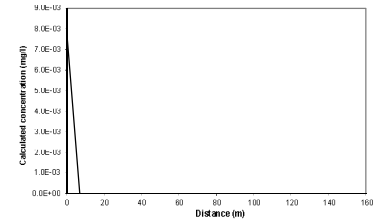
Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	ax	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	az	0.00E+00	1.39E+01	6.00E+00	m
Vertical dispersivity	ay	0.00E+00	1.39E+00	6.75E-01	rr
Vertical dispersivity	ay	0.00E+00	1.39E-01	6.75E-02	rr

Note values of dispersivity must be > 0

For calculated value, assumes ax = 0.1 * x, az = 0.01 * x, ay = 0.001 * x
Xu & Eckstein (1995) report ax = 0.83(log₁₀)^{2.44H}, az = ax/10, ay = ax/100 are assumed



Calculated concentrations for distance-concentration graph

Ogata Banks
From calculation sheet

Distance	Concentration
	mg/l
0	7.7E-03
7.0	2.35E-42
13.9	7.13E-82
20.9	2.16E-121
27.8	6.56E-161
34.8	1.99E-200
41.7	6.04E-240
48.7	1.83E-279
55.6	0.00E+00
62.6	0.00E+00
69.5	0.00E+00
76.5	0.00E+00
83.4	0.00E+00
90.4	0.00E+00
97.3	0.00E+00
104.3	0.00E+00
111.2	0.00E+00
118.2	0.00E+00
125.1	0.00E+00
132.1	0.00E+00
139.0	0.00E+00

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Bis(2-ethylhexyl) phthalate		
Target Concentration (C_T)	0.0013	mg/l	Origin of C_T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.

Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Bis(2-ethylhexyl) phthalate	from Level 1
Target Concentration	C _t 1.30E-03	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	1.27E-01	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	1.00E+04	days	See justification table
Calculated decay rate	λ	8.03E-05	days ⁻¹	
Width of plume in aquifer at source (perpendicular to flow)	Sz	8.00E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	x	1.39E+02	rr	See justification table
Distance to compliance point	z	0.00E+00	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options				
Partition coefficient	Kd	5.39E+04	l/kg	see options
Longitudinal dispersivity	αx	1.39E+01	m	see options
Transverse dispersivity	αz	1.39E+00	m	see options
Vertical dispersivity	αy	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d	
Retardation factor	Rf	1.17E+06	fraction	
Decay rate used	λ	8.93E-05	d ⁻¹	
Rate of contaminant flow due to retardation	u	4.90E-08	m/d	
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	0.00E+00	mg/l	
Attenuation factor (one way vertical dispersion, COC/ED)	AF	breakthrough at compliance point		

Remedial Targets

Remedial Target	No Impact	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point	C _{eq} /C ₀	0.00E+00	mg/l Ogata Banks
after		1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)

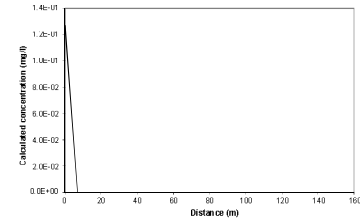
Soil water partition coefficient	Kd	5.39E+04	l/kg
Entry for non-polar organic chemicals (option)			
Fraction of organic carbon in aquifer	foc	8.18E-01	fraction
Organic carbon partition coefficient	Koc	8.74E+04	l/kg
Entry for ionic organic chemicals (option)			
Sorption coefficient for related species	K _{oc,n}	8.00E+00	l/kg
Sorption coefficient for ionised species	K _{oc,i}	8.00E+00	l/kg
pH value	pH	8.00E+00	l/kg
acid dissociation constant	pKa	8.00E+00	l/kg
Fraction of organic carbon in aquifer	foc	8.00E+00	fraction
Soil water partition coefficient	Kd	5.39E+04	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	αx	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	αz	0.00E+00	1.39E+01	5.72E+00	m
Vertical dispersivity	αy	0.00E+00	1.39E+00	5.72E-01	rr
Vertical dispersivity	αy	8.00E+00	1.39E-01	5.72E-02	rr

Note values of dispersivity must be > 0
For calculated value, assumes αx = 0.1 * x, αz = 0.01 * x, αy = 0.001 * x
Xu & Eckstein (1995) report αx = 0.83(log₁₀)^{2.44H}, αz = αx/10, αy = αx/100 are assumed



Calculated concentrations for distance-concentration graph

Ogata Banks	From calculation sheet	
Distance	Concentration	
	mg/l	
0	1.3E-01	
7.0	5.72E-02	
13.9	2.57E-02	
20.9	1.16E-02	
27.8	5.22E-03	
34.8	2.35E-03	
41.7	1.06E-03	
48.7	4.76E-04	
55.6	2.14E-04	
62.6	9.64E-05	
69.5	4.34E-05	
76.5	0.00E+00	
83.4	0.00E+00	
90.4	0.00E+00	
97.3	0.00E+00	
104.3	0.00E+00	
111.2	0.00E+00	
118.2	0.00E+00	
125.1	0.00E+00	
132.1	0.00E+00	
139.0	0.00E+00	

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Cadmium		
Target Concentration (C_T)	0.00008 mg/l	Origin of C_T :	EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

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Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Cadmium	from Level 1
Target Concentration	$8.00E-05$	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
-------------	------------------------------

Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C_0	$4.61E-03$	mg/l	See justification table
Half life for degradation of contaminant in water	$t_{1/2}$	$1.00E+09$	days	See justification table
Calculated decay rate	λ	$6.93E-10$	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	$5.50E+02$	rr	See justification table
Plume thickness at source	Sy	$2.50E+01$	rr	See justification table
Saturated aquifer thickness	da	$3.00E+01$	rr	See justification table
Bulk density of aquifer materials	ρ	$2.17E+00$	g/cm ³	See justification table
Effective porosity of aquifer	n	$1.00E-01$	fraction	See justification table
Hydraulic gradient	i	$1.20E-02$	fraction	See justification table
Hydraulic conductivity of aquifer	K	$4.77E-01$	m/s	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	x	$1.39E+02$	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	z	$0.00E+00$	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	$0.00E+00$	rr	See justification table
Time since pollutant entered groundwater	t	$1.00E+100$	days	time variant options only

Parameters values determined from options				
Partition coefficient	Kd	$2.56E+03$	l/kg	see options
Longitudinal dispersivity	αx	$1.39E+01$	m	see options
Transverse dispersivity	αz	$1.39E+00$	m	see options
Vertical dispersivity	αy	$1.39E-01$	m	see options

Calculated Parameters

Groundwater flow velocity	v	$5.72E-02$	m/d
Retardation factor	Rf	$5.56E+04$	fraction
Decay rate used	λ	$8.93E-10$	d ⁻¹
Rate of contaminant flow due to retardation	u	$1.03E-06$	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C_{eq}	$4.20E-03$	mg/l
Attenuation factor (one way vertical dispersion, COCED)	AF	$1.10E+00$	

Remedial Targets

Remedial Target	$8.78E-05$	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C_{eq}/C_0	$4.20E-03$	mg/l Ogata Banks
		$1.0E+100$	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is $9.9E+09$.

Select Method for deriving Partition Co-efficient (using pull down menu)

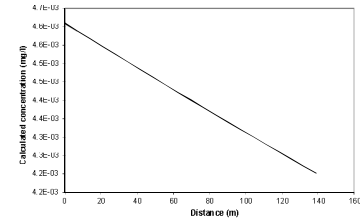
User specified value for partition coefficient

Entry if specify partition coefficient (option)	Kd	$2.56E+03$	l/kg
Soil water partition coefficient	Kd	$2.56E+03$	l/kg
Entry for non-polar organic chemicals (option)	foc	$1.00E-01$	fraction
Fraction of organic carbon in aquifer	foc	$1.00E-01$	fraction
Organic carbon partition coefficient	Koc	$1.00E+01$	l/kg
Entry for ionic organic chemicals (option)	$K_{oc,n}$	$1.00E+01$	l/kg
Sorption coefficient for related species	$K_{oc,n}$	$1.00E+01$	l/kg
Sorption coefficient for ionised species	$K_{oc,n}$	$1.00E+01$	l/kg
pH value	pH	$1.00E+01$	l/kg
acid dissociation constant	pKa	$1.00E+01$	fraction
Fraction of organic carbon in aquifer	foc	$1.00E-01$	fraction
Soil water partition coefficient	Kd	$2.56E+03$	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	αx	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	αz	$0.00E+00$	$1.39E+01$	$5.20E+00$	m
Vertical dispersivity	αy	$0.00E+00$	$1.39E+00$	$5.72E-01$	rr
Note values of dispersivity must be > 0					
For calculated value, assumes $\alpha x = 0.1 * x$, $\alpha z = 0.01 * z$, $\alpha y = 0.001 * y$					
Xu & Eckstein (1995) report $\alpha x = 0.83(\log_{10} t)^{0.41H}$, $\alpha z = \alpha x/10$, $\alpha y = \alpha x/100$ are assumed					



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as $9.0E+09$.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O_2 , NO_3 , SO_4 etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name: M54 M6 Link Road

Site Address:

Completed by: Gabriella Barnes

Date: 02-Dec-19

Version: 1

Contaminant Chromium (hexavalent)

Target Concentration (C_T) 0.0034 mg/l

Origin of C_T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

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Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Chromium (hexavalent)	from Level 1
Target Concentration	C _r 3.40E-03	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
-------------	------------------------------

Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	2.78E-02	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	1.00E+09	days	See justification table
Calculated decay rate	λ	6.93E-10	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.50E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	x	1.39E+02	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	z	0.00E+00	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options

Partition coefficient	Kd	4.80E+03	l/kg	see options
Longitudinal dispersivity	α _x	1.39E+01	m	see options
Transverse dispersivity	α _z	1.39E+00	m	see options
Vertical dispersivity	α _y	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d
Retardation factor	Rf	1.04E+05	fraction
Decay rate used	λ	6.93E-10	d ⁻¹
Rate of contaminant flow due to retardation	u	5.50E-07	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	2.34E-02	mg/l
Attenuation factor (one way vertical dispersion, COCED)	AF	1.19E+00	

Remedial Targets

Remedial Target	4.04E-03	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C _{eq} /C ₀ 2.34E-02	mg/l	Ogata Banks
	1.0E+100	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

User specified value for partition coefficient

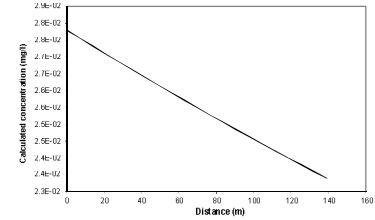
Entry if specify partition coefficient (option)	Kd	4.80E+03	l/kg
Soil water partition coefficient	K _d	4.80E+03	l/kg
Entry for non-polar organic chemicals (option)	foc	1.00E-01	fraction
Fraction of organic carbon in aquifer	foc	1.00E-01	fraction
Organic carbon partition coefficient	K _{oc}	1.00E+01	l/kg
Entry for ionic organic chemicals (option)	K _{oc,n}	1.00E+01	l/kg
Sorption coefficient for related species	K _{oc,n}	1.00E+01	l/kg
Sorption coefficient for ionised species	K _{oc,n}	1.00E+01	l/kg
pH value	pH	1.00E+01	l/kg
acid dissociation constant	pKa	1.00E+01	fraction
Fraction of organic carbon in aquifer	foc	1.00E-01	fraction
Soil water partition coefficient	Kd	4.80E+03	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	α _x	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	α _z	0.00E+00	1.39E+01	5.00E+00	m
Vertical dispersivity	α _y	0.00E+00	1.39E+00	5.72E-01	rr
Vertical dispersivity	α _y	0.00E+00	1.39E-01	5.72E-02	rr

Note values of dispersivity must be > 0
For calculated value, assumes α_x = 0.1 * x, α_z = 0.01 * x, α_y = 0.001 * x
Xu & Eckstein (1995) report α_x = 0.83(log₁₀)^{2.41H}, α_z = α_x/10, α_y = α_x/100 are assumed



Calculated concentrations for distance-concentration graph

Distance	Concentration
0	2.8E-02
7.0	2.76E-02
13.9	2.73E-02
20.9	2.71E-02
27.8	2.69E-02
34.8	2.66E-02
41.7	2.64E-02
48.7	2.62E-02
55.6	2.59E-02
62.6	2.57E-02
69.5	2.55E-02
76.5	2.53E-02
83.4	2.51E-02
90.4	2.49E-02
97.3	2.48E-02
104.3	2.44E-02
111.2	2.42E-02
118.2	2.40E-02
125.1	2.38E-02
132.1	2.36E-02
139.0	2.34E-02

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes	Version:	1
Date:	02-Dec-19		
Contaminant	Copper		
Target Concentration (C_T)	0.001	mg/l	Origin of C_T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

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The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note



Input Parameters (using pull down menu)

Contaminant **Copper** from Level 1
Target Concentration **C_t** **1.00E-03** mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks Equations in HRA publication

Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	1.24E-02	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	1.00E+09	days	See justification table
Calculated decay rate	λ	8.93E-10	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.50E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	x	1.39E+02	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	z	0.00E+00	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Partition coefficient	Kd	3.50E+01	l/kg	see options
Longitudinal dispersivity	αx	1.39E+01	m	see options
Transverse dispersivity	αz	1.39E+00	m	see options
Vertical dispersivity	αy	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d
Retardation factor	Rf	7.61E+02	fraction
Decay rate used	λ	8.93E-10	d ⁻¹
Rate of contaminant flow due to retardation	u	7.53E-05	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{eq}	1.24E-02	mg/l
Attenuation factor (one way vertical dispersion, COCED)	AF	1.00E+00	

Remedial Targets

Remedial Target	1.00E-03	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C _{eq} /C ₀	1.24E-02	mg/l
		1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+09.

Select Method for deriving Partition Co-efficient (using pull down menu)

User specified value for partition coefficient

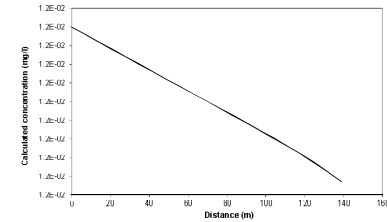
Entry if specify partition coefficient (option)	Kd	3.50E+01	l/kg
Soil water partition coefficient	Kd	3.50E+01	l/kg
Entry for non-polar organic chemicals (option)	foc	1.00E-03	fraction
Fraction of organic carbon in aquifer	foc	1.00E-03	fraction
Organic carbon partition coefficient	Koc	1.00E+00	l/kg
Entry for ionic organic chemicals (option)	Koc,n	1.00E+00	l/kg
Sorption coefficient for related species	Koc,n	1.00E+00	l/kg
Sorption coefficient for ionised species	Koc,n	1.00E+00	l/kg
pH value	pH	1.00E+00	l/kg
acid dissociation constant	pKa	1.00E+00	fraction
Fraction of organic carbon in aquifer	foc	1.00E-03	fraction
Soil water partition coefficient	Kd	3.50E+01	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	αx	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	αz	0.00E+00	1.39E+01	5.72E+00	m
Vertical dispersivity	αy	0.00E+00	1.39E+00	5.72E-01	rr
Vertical dispersivity	αy	0.00E+00	1.39E-01	5.72E-02	rr

Note values of dispersivity must be > 0
For calculated value, assumes αx = 0.1 * x, αz = 0.01 * x, αy = 0.001 * x
Xu & Eckstein (1995) report αx = 0.83(log₁₀)^{2.44}, αz = αx/10, αy = αx/100 are assumed



Calculated concentrations for distance-concentration graph

Ogata Banks	From calculation sheet
Distance	Concentration
0	1.2E-02
7.0	1.24E-02
13.9	1.24E-02
20.9	1.24E-02
27.8	1.24E-02
34.8	1.24E-02
41.7	1.24E-02
48.7	1.24E-02
55.6	1.24E-02
62.6	1.24E-02
69.5	1.24E-02
76.5	1.24E-02
83.4	1.24E-02
90.4	1.24E-02
97.3	1.24E-02
104.3	1.24E-02
111.2	1.24E-02
118.2	1.24E-02
125.1	1.24E-02
132.1	1.24E-02
139.0	1.24E-02

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+09.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name: M54 M6 Link Road

Site Address:

Completed by: Gabriella Barnes

Date: 02-Dec-19

Version: 1

Contaminant Ethylbenzene

Target Concentration (C_T) 0.02

mg/l

Origin of C_T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

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It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Ethylbenzene	from Level 1
Target Concentration	C _t 2.00E-02	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants

Apply degradation rate to pollutants in all phases (e.g. field derived value)

Initial contaminant concentration in groundwater at plume core	C ₀	4.50E-02	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	5.00E+02	days	See justification table
Calculated decay rate	λ	1.39E-03	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	8.00E+02	rr	See justification table
Plume thickness at source	Sy	2.50E+01	rr	See justification table
Saturated aquifer thickness	da	3.00E+01	rr	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	i	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/s	See justification table
Distance to compliance point	x	1.39E+02	rr	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	0.00E+00	rr	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	rr	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options

Partition coefficient	Kd	2.75E+02	l/kg	see options
Longitudinal dispersivity	α _x	1.39E+01	m	see options
Transverse dispersivity	α _z	1.39E+00	m	see options
Vertical dispersivity	α _y	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d
Retardation factor	Rf	5.98E+03	fraction
Decay rate used	λ	1.39E-03	days ⁻¹
Rate of contaminant flow due to retardation	u	9.58E-06	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C ₉₉	1.03E-194	mg/l
Attenuation factor (one way vertical dispersion, COCED)	AF	4.37E+192	

Remedial Targets

Remedial Target	8.74E+190	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C ₉₉ /C ₀ 1.03E-194	mg/l	Ogata Banks
	1.0E+100	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

Calculate for non-polar organic chemicals

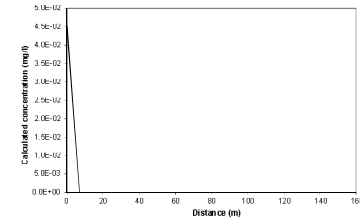
Entry if specify partition coefficient (option)

Soil water partition coefficient	Kd	2.75E+02	l/kg
Entry for non-polar organic chemicals (option)			
Fraction of organic carbon in aquifer	foc	6.18E-01	fraction
Organic carbon partition coefficient	Koc	4.47E+02	l/kg
Entry for ionic organic chemicals (option)			
Sorption coefficient for related species	K _{oc,n}	2.75E+02	l/kg
Sorption coefficient for ionised species	K _{oc,i}	2.75E+02	l/kg
pH value	pH	7.00E+00	
acid dissociation constant	pKa	2.75E+02	fraction
Fraction of organic carbon in aquifer	foc	6.18E-01	fraction
Soil water partition coefficient	Kd	2.75E+02	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10% 1% 0.1% of pathway length

Longitudinal dispersivity	α _x	Enter value	Calc value	Xu & Eckstein	rr
Transverse dispersivity	α _z	0.00E+00	1.39E+01	2.00E+00	m
Vertical dispersivity	α _y	0.00E+00	1.39E+00	5.72E-01	rr
Note values of dispersivity must be > 0					
For calculated value, assumes α _x = 0.1 * x, α _z = 0.01 * x, α _y = 0.001 * x					
Xu & Eckstein (1995) report α _x = 0.83(log ₁₀) ^{2.44H} , α _z = α _x /10, α _y = α _x /100 are assumed					



Calculated concentrations for distance-concentration graph

Ogata Banks
From calculation sheet
Distance Concentration

0	4.5E-02
7.0	1.05E-11
13.9	2.45E-21
20.9	5.72E-31
27.8	1.33E-40
34.8	3.11E-50
41.7	7.26E-60
48.7	1.69E-69
55.6	3.95E-79
62.6	9.23E-89
69.5	2.15E-98
76.5	5.02E-108
83.4	1.17E-117
90.4	2.74E-127
97.3	6.38E-137
104.3	1.49E-146
111.2	3.47E-156
118.2	8.11E-166
125.1	1.89E-175
132.1	4.41E-185
139.0	1.03E-194

Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+99.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc then an alternative solution should be used.

Site being assessed	K94 M6 Link Road
Completed by	Gabriella Barnes
Date	07/12/2018
Version	



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Fluoranthene		
Target Concentration (C _T)	0.0000063	mg/l	Origin of C _T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.

Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Fluoranthene	from Level 1
Target Concentration	$6.30E-06$	mg/l from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived values)
--

Initial contaminant concentration in groundwater at plume core	C_0	$1.10E-02$	mg/l	See justification table
Half life for degradation of contaminant in water	$t_{1/2}$	$5.00E+03$	days	See justification table
Calculated decay rate	λ	$1.39E-04$	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	S_z	$5.50E+02$	m	See justification table
Plume thickness at source	S_y	$2.50E+01$	m	See justification table
Saturated aquifer thickness	d_a	$3.00E+01$	m	See justification table
Bulk density of aquifer materials	ρ	$2.17E+00$	g/cm ³	See justification table
Effective porosity of aquifer	n	$1.00E-01$	fraction	See justification table
Hydraulic gradient	I	$1.20E-02$	fraction	See justification table
Hydraulic conductivity of aquifer	K	$4.77E-01$	m/d	See justification table
Distance to compliance point	x	$1.39E+02$	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	$0.00E+00$	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	$0.00E+00$	m	See justification table
Time since pollutant entered groundwater	t	$1.00E+100$	days	time variant options only
Parameters values determined from options				
Partition coefficient	K_d	$1.12E+04$	l/kg	see options
Longitudinal dispersivity	α_x	$1.39E+01$	m	see options
Transverse dispersivity	α_z	$1.39E+00$	m	see options
Vertical dispersivity	α_y	$1.39E-01$	m	see options

Calculated Parameters

Groundwater flow velocity	V	$5.72E-02$	m/d
Retardation factor	R_f	$2.43E+05$	fraction
Decay rate used	λ	$1.39E-04$	d ⁻¹
Rate of contaminant flow due to retardation	u	$2.35E-07$	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C_{ED}	$0.00E+00$	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	breakthrough at compliance point	

Remedial Targets

Remedial Target	No impact	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C_{ED}/C_0	$0.00E+00$	mg/l
		$1.0E+100$	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is $9.9E+99$.

Select Method for deriving Partition Co-efficient (using pull down menu)

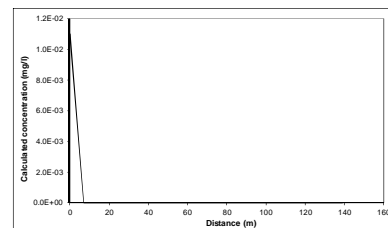
Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)		
Soil water partition coefficient	K_d	l/kg
Entry for non-polar organic chemicals (option)		
Fraction of organic carbon in aquifer	f_{oc}	fraction
Organic carbon partition coefficient	K_{oc}	l/kg
Entry for ionic organic chemicals (option)		
Sorption coefficient for related species	K_{ow}	l/kg
Sorption coefficient for ionised species	K_{ow}	l/kg
pH value	pH	
acid dissociation constant	pKa	fraction
Fraction of organic carbon in aquifer	f_{oc}	
Soil water partition coefficient	K_d	$1.12E+04$ l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	α_x	Enter value	Calc value	α_x & Eckstein	m
Transverse dispersivity	α_z	$0.00E+00$	$1.39E+01$	$0.23E+03$	m
Vertical dispersivity	α_y	$0.00E+00$	$1.39E+01$	$0.23E+02$	m
Note values of dispersivity must be > 0					
For calculated value, assumes $\alpha_x = 0.1 * x$, $\alpha_z = 0.01 * x$, $\alpha_y = 0.001 * x$					
α_x & Eckstein (1995) report $\alpha_x = 0.83(\log_{10} x)^{0.414}$; $\alpha_z = \alpha_x/10$, $\alpha_y = \alpha_x/100$ are assumed					



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as $9.0E+99$.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed: M54 M6 Link Road
Completed by: Gabriella Barnes
Date: 02/12/2019
Version: 1



Calculated concentrations for distance-concentration graph

Distance	Concentration
0	1.1E-02
7.0	3.15E-22
13.9	9.00E-42
20.9	2.57E-61
27.8	7.36E-81
34.8	2.10E-100
41.7	6.02E-120
48.7	1.72E-139
55.6	4.92E-159
62.6	1.41E-178
69.5	4.03E-198
76.5	1.15E-217
83.4	3.29E-237
90.4	9.42E-257
97.3	2.69E-276
104.3	7.71E-296
111.2	0.00E+00
118.2	0.00E+00
125.1	0.00E+00
132.1	0.00E+00
139.0	0.00E+00



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Naphthalene		
Target Concentration (C _T)	0.002	mg/l	Origin of C _T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.

Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Naphthalene	From Level 1
Target Concentration	C_T 2.00E-03	mg/l From Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
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Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived values)
--

Initial contaminant concentration in groundwater at plume core	C_0	7.48E-03	mg/l	See justification table
Half life for degradation of contaminant in water	$t_{1/2}$	1.00E+03	days	See justification table
Calculated decay rate	λ	6.93E-04	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	S_z	8.00E+02	m	See justification table
Plume thickness at source	S_y	2.50E+01	m	See justification table
Saturated aquifer thickness	d_a	3.00E+01	m	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	I	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/d	See justification table
Distance to compliance point	x	1.39E+02	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	0.00E+00	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	m	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only

Parameters values determined from options				
Partition coefficient	K_d	3.98E+02	l/kg	see options
Longitudinal dispersivity	α_x	1.39E+01	m	see options
Transverse dispersivity	α_z	1.39E+00	m	see options
Vertical dispersivity	α_y	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	V	5.72E-02	m/d
Retardation factor	R_f	8.63E+03	fraction
Decay rate used	λ	6.93E-04	d ⁻¹
Rate of contaminant flow due to retardation	U	6.63E-06	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C_{ED}	3.09E-166	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	2.43E+163	

Remedial Targets

Remedial Target	4.85E+160	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			

Distance to compliance point	139	m
Concentration of contaminant at compliance point after	C_{ED}/C_0 3.09E-166	mg/l
	1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

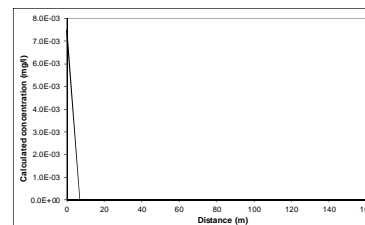
Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)		
Soil water partition coefficient	K_d	3.98E+02 l/kg
Entry for non-polar organic chemicals (option)		
Fraction of organic carbon in aquifer	f_{oc}	6.16E-01 fraction
Organic carbon partition coefficient	K_{oc}	6.46E+02 l/kg
Entry for ionic organic chemicals (option)		
Sorption coefficient for related species	K_{ow}	l/kg
Sorption coefficient for ionised species	K_{ow}	l/kg
pH value	pH	
acid dissociation constant	pKa	fraction
Fraction of organic carbon in aquifer	f_{oc}	
Soil water partition coefficient	K_d	3.98E+02 l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	α_x	1.39E+01	1.39E+01	1.39E+01	1.39E+01	m
Transverse dispersivity	α_z	0.00E+00	1.39E+00	1.39E+00	1.39E+00	m
Vertical dispersivity	α_y	0.00E+00	1.39E-01	1.39E-01	1.39E-01	m
Note values of dispersivity must be > 0						
For calculated value, assumes $\alpha_x = 0.1 * x$, $\alpha_z = 0.01 * x$, $\alpha_y = 0.001 * x$						
Xu & Eckstein (1995) report $\alpha_x = 0.83(\log_{10} x)^{0.414}$; $\alpha_z = \alpha_x/10$, $\alpha_y = \alpha_x/100$ are assumed						



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+99.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Calculated concentrations for distance-concentration graph

Ogata Banks		
From calculation sheet		
Distance	Concentration	mg/l
0	7.5E-03	
7.0	5.07E-11	
13.9	3.44E-19	
20.9	2.33E-27	
27.8	1.58E-35	
34.8	1.07E-43	
41.7	7.23E-52	
48.7	4.90E-60	
55.6	3.32E-68	
62.6	2.25E-76	
69.5	1.52E-84	
76.5	1.03E-92	
83.4	6.98E-101	
90.4	4.72E-109	
97.3	3.20E-117	
104.3	2.17E-125	
111.2	1.47E-133	
118.2	9.94E-142	
125.1	6.73E-150	
132.1	4.56E-158	
139.0	3.09E-166	

Site being assessed: M54 M6 Link Road
Completed by: Gabriella Barnes
Date: 02/12/2019
Version: 1



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Nickel		
Target Concentration (C_T)	0.004	mg/l	Origin of C_T: EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

Worksheet options are identified by brown background and employ a pull-down menus. Data entry are identified as blue background.

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Data carried forward from an earlier worksheet are identified by a light green background

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Nickel	From Level 1
Target Concentration	C_T 4.00E-03	mg/l From Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
-------------	------------------------------

Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived values)
--

Initial contaminant concentration in groundwater at plume core	C_0 2.30E-02	mg/l	See justification table
Half life for degradation of contaminant in water	$t_{1/2}$ 1.00E+00	days	See justification table
Calculated decay rate	λ 6.93E-10	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	S_z 5.50E+02	m	See justification table
Plume thickness at source	S_y 2.50E+01	m	See justification table
Saturated aquifer thickness	d_a 3.00E+01	m	See justification table
Bulk density of aquifer materials	ρ 2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n 1.00E-01	fraction	See justification table
Hydraulic gradient	I 1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K 4.77E-01	m/d	See justification table
Distance to compliance point	x 1.39E+02	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z 0.00E+00	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y 0.00E+00	m	See justification table
Time since pollutant entered groundwater	t 1.00E+100	days	time variant options only

Parameters values determined from options

Partition coefficient	K_d 2.00E+03	l/kg	see options
Longitudinal dispersivity	α_x 1.39E+01	m	see options
Transverse dispersivity	α_z 1.39E+00	m	see options
Vertical dispersivity	α_y 1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	v	5.72E-02	m/d
Retardation factor	R_f	4.34E+04	fraction
Decay rate used	λ	6.93E-10	d ⁻¹
Rate of contaminant flow due to retardation	u	1.32E-06	m/d
Contaminant concentration at distance x , assuming one-way vertical dispersion	C_{ED}	2.16E-02	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	1.08E+00	

Remedial Targets

Remedial Target	4.30E-03	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C_{ED}/C_0 2.16E-02	mg/l	Ogata Banks
	1.0E+100	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

User specified value for partition coefficient

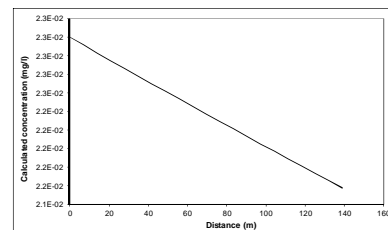
Entry if specify partition coefficient (option)

Soil water partition coefficient	K_d 2.00E+03	l/kg
Entry for non-polar organic chemicals (option)		
Fraction of organic carbon in aquifer	f_{oc}	fraction
Organic carbon partition coefficient	K_{oc}	l/kg
Entry for ionic organic chemicals (option)		
Sorption coefficient for related species	K_{ow}	l/kg
Sorption coefficient for ionised species	K_{ow}	l/kg
pH value	pH	fraction
acid dissociation constant	pKa	fraction
Fraction of organic carbon in aquifer	f_{oc}	fraction
Soil water partition coefficient	K_d 2.00E+03	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	α_x 1.39E+01	1.39E+01	5.23E+01	m
Transverse dispersivity	α_z 0.00E+00	1.39E+00	5.23E-01	m
Vertical dispersivity	α_y 0.00E+00	1.39E-01	5.23E-02	m
Note values of dispersivity must be > 0				
For calculated value, assumes $\alpha_x = 0.1 * x$, $\alpha_z = 0.01 * x$, $\alpha_y = 0.001 * x$				
Xu & Eckstein (1995) report $\alpha_x = 0.83(\log_{10} x)^{0.414}$; $\alpha_z = \alpha_x/10$, $\alpha_y = \alpha_x/100$ are assumed				



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+99.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed: M54 M6 Link Road
Completed by: Gabriella Barnes
Date: 02/12/2019
Version: 1



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Toll Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Phenol		
Target Concentration (C _T)	0.0077	mg/l	Origin of C _T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

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The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Phenol	from Level 1
Target Concentration	$7.70E-03$	from Level 1
C_T		

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks Equations in HRA publication

Approach for simulating vertical dispersion:

Simulate vertical dispersion in 2 directions

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived v)

Initial contaminant concentration in groundwater at plume core	C_0	$8.70E-02$	mg/l	Source of parameter value
Half life for degradation of contaminant in water	$t_{1/2}$	$3.50E+02$	days	See justification table
Calculated decay rate	λ	$1.99E-03$	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	$8.00E+02$	m	See justification table
Plume thickness at source	Sy	$2.50E+01$	m	See justification table
Saturated aquifer thickness	da	$3.00E+01$	m	See justification table
Bulk density of aquifer materials	ρ	$2.17E+00$	g/cm ³	See justification table
Effective porosity of aquifer	n	$1.00E-01$	fraction	See justification table
Hydraulic gradient	i	$1.20E-02$	fraction	See justification table
Hydraulic conductivity of aquifer	K	$4.77E-01$	m/d	See justification table
Distance to compliance point	x	$1.39E+02$	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	$0.00E+00$	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	$0.00E+00$	m	See justification table
Time since pollutant entered groundwater	t	$1.00E+100$	days	time variant options only
Parameters values determined from options				
Partition coefficient	Kd	$5.13E+01$	l/kg	see options
Longitudinal dispersivity	ax	$1.39E+01$	m	see options
Transverse dispersivity	az	$1.39E+00$	m	see options
Vertical dispersivity	ay	$1.39E-01$	m	see options

Calculated Parameters

Groundwater flow velocity	v	$5.72E-02$	m/d
Retardation factor	Rf	$1.11E+03$	fraction
Decay rate used	λ	$1.99E-03$	d ⁻¹
Rate of contaminant flow due to retardation	u	$5.14E-05$	m/d
Contaminant concentration at distance x, assuming two-way vertical dispersion	C_{ED}	$3.82E-100$	mg/l
Attenuation factor (two way vertical dispersion, CO/CED)	AF	$2.28E+98$	

Remedial Targets

Remedial Target	$1.76E+96$	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point	$3.82E-100$	mg/l	Ogata Banks
after	$1.0E+100$	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is $9.9E+99$.

Select Method for deriving Partition Co-efficient (using pull down menu)

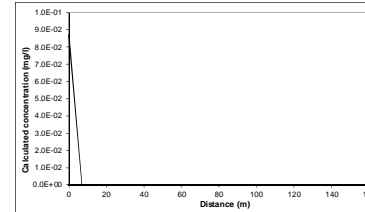
Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)	Kd		l/kg
Soil water partition coefficient	Kd		l/kg
Entry for non-polar organic chemicals (option)	foc	$6.16E-01$	fraction
Fraction of organic carbon in aquifer	foc		
Organic carbon partition coefficient	Koc	$8.32E+01$	l/kg
Entry for ionic organic chemicals (option)	K _{oc,0}		l/kg
Sorption coefficient for related species	K _{oc,0}		l/kg
Sorption coefficient for ionised species	K _{oc,i}		l/kg
pH value	pH		
acid dissociation constant	pKa		
Fraction of organic carbon in aquifer	foc		fraction
Soil water partition coefficient	Kd	$5.13E+01$	l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

		Enter value	Calc value Xu & Eckstein	m
Longitudinal dispersivity	ax	0.00E+00	1.39E+01	1.39E+01
Transverse dispersivity	az	0.00E+00	1.39E+00	1.39E+00
Vertical dispersivity	ay	0.00E+00	1.39E-01	1.39E-01
Note values of dispersivity must be > 0				
For calculated value, assumes ax = 0.1 * x, az = 0.01 * x, ay = 0.001 * x				
Xu & Eckstein (1995) report ax = 0.83(log ₁₀ x) ^{2.414} ; az = ax/10, ay = ax/100 are assumed				



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source. Three solution methods are included; the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action. Note if contaminant is not subject to first order degradation, then set half life as $9.0E+99$.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used.

Site being assessed: M6 M6 Toll Link Road

Completed by: Gabriela Barnes

Date: #####

Version: 1

Calculated concentrations for distance-concentration graph

Ogata Banks
From calculation sheet
Distance Concentration

	mg/l
0	8.7E-02
7.0	1.05E-06
13.9	1.28E-11
20.9	1.54E-16
27.8	1.87E-21
34.8	2.26E-26
41.7	2.74E-31
48.7	3.32E-36
55.6	4.01E-41
62.6	4.86E-46
69.5	5.87E-51
76.5	7.09E-56
83.4	8.56E-61
90.4	1.03E-65
97.3	1.25E-70
104.3	1.50E-75
111.2	1.81E-80
118.2	2.18E-85
125.1	2.63E-90
132.1	3.17E-95
139.0	3.82E-100



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Xylene Total		
Target Concentration (C _T)	0.03	mg/l	Origin of C _T : EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

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The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)	Variable	Value	Unit	Source
Contaminant	Xylene Total			from Level 1
Target Concentration	C _T	3.00E-02	mg/l	from Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
-------------	------------------------------

Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived values)
--

Initial contaminant concentration in groundwater at plume core	C ₀	9.10E-02	mg/l	See justification table
Half life for degradation of contaminant in water	t _{1/2}	5.00E+02	days	See justification table
Calculated decay rate	λ	1.39E-03	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	Sz	5.50E+02	m	See justification table
Plume thickness at source	Sy	2.50E+01	m	See justification table
Saturated aquifer thickness	da	3.00E+01	m	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	I	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/d	See justification table
Distance to compliance point	x	1.39E+02	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	0.00E+00	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	m	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only
Parameters values determined from options				
Partition coefficient	Kd	2.79E+02	l/kg	see options
Longitudinal dispersivity	ax	1.39E+01	m	see options
Transverse dispersivity	az	1.39E+00	m	see options
Vertical dispersivity	ay	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	V	5.72E-02	m/d
Retardation factor	Rf	6.06E+03	fraction
Decay rate used	λ	1.39E-03	d ⁻¹
Rate of contaminant flow due to retardation	u	9.44E-06	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C _{ED}	7.72E-196	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	1.18E+194	

Remedial Targets

Remedial Target	3.54E+192	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C _{ED} /C ₀	7.72E-196	mg/l
	after	1.0E+100	days

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

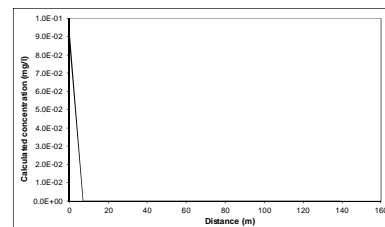
Calculate for non-polar organic chemicals

Entry if specify partition coefficient (option)		
Soil water partition coefficient	Kd	
Entry for non-polar organic chemicals (option)		
Fraction of organic carbon in aquifer	foc	6.16E-01
Organic carbon partition coefficient	Koc	4.54E+02
Entry for ionic organic chemicals (option)		
Sorption coefficient for related species	K _{ow}	
Sorption coefficient for ionised species	K _{ow}	
pH value	pH	
acid dissociation constant	pKa	
Fraction of organic carbon in aquifer	foc	
Soil water partition coefficient	Kd	2.79E+02

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	ax	1.39E+01	1.39E+01	5.23E+01	m
Transverse dispersivity	az	0.00E+00	1.39E+00	5.23E-01	m
Vertical dispersivity	ay	0.00E+00	1.39E-01	5.23E-02	m
Note values of dispersivity must be > 0					
For calculated value, assumes ax = 0.1 * x, az = 0.01 * x, ay = 0.001 * x					
Xu & Eckstein (1995) report ax = 0.83(log ₁₀ x) ^{0.414} ; az = ax/10, ay = ax/100 are assumed					



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

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By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+99.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Site being assessed: M54 M6 Link Road
Completed by: Gabriella Barnes
Date: 02/12/2019
Version: 1



Hydrogeological risk assessment for land contamination

Remedial Targets Worksheet , Release 3.2

First released: 2006. Version 3.2: January 2013

This worksheet has been produced in combination with the document 'Remedial Targets Methodology: Hydrogeological risk assessment for land contamination (Environment Agency 2006).

Users of this worksheet should always refer to the User Manual to the Remedial Targets Methodology and to relevant guidance on UK legislation and policy, in order to understand how this procedure should be applied in an appropriate context.

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IMPORTANT: To enable MS Excel worksheet, click Tools, Add -Ins, Analysis Tool Pak and Analysis Tool Pak-VBA (to calculate error functions)

Details to be completed for each assessment

Site Name:	M54 M6 Link Road		
Site Address:			
Completed by:	Gabriella Barnes		
Date:	02-Dec-19	Version:	1
Contaminant	Zinc		
Target Concentration (C_T)	0.0109	mg/l	Origin of C_T: EQS

This worksheet can be used to determine remedial targets for soils (Worksheets Level 1 Soil, Level 2 and Level 3 Soil) or to determine remedial targets for groundwater (Level 3 Groundwater). For Level 3, parameter values must be entered separately dependent on whether the assessment is for soil or groundwater. For soil, remedial targets are calculated as either mg/kg (for comparison with soil measurements) or mg/l (for comparison with leaching tests or pore water concentrations).

Site details entered on this page are automatically copied to Level 1, 2 and 3 Worksheets.

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The spreadsheet also includes a porosity calculation worksheet, a soil impact calculation worksheet and a worksheet that performs some simple hydrogeological calculations.

R&D Publication 20 Remedial Targets Worksheet, Release 3.2

Level 3 - Groundwater

See Note

Input Parameters (using pull down menu)

Contaminant	Zinc	From Level 1
Target Concentration	C_T 1.00E-02	mg/l From Level 1

Select analytical solution (click on brown cell below, then on pull-down menu)

Ogata Banks	Equations in HRA publication
-------------	------------------------------

Approach for simulating vertical dispersion:

Simulate vertical dispersion in 1 direction

Select nature of decay rate (click on brown cell below, then on pull-down menu)

Approach for simulating degradation of pollutants:

Apply degradation rate to pollutants in all phases (e.g. field derived values)
--

Initial contaminant concentration in groundwater at plume core	C_0	4.01E-02	mg/l	See justification table
Half life for degradation of contaminant in water	$t_{1/2}$	1.00E+00	days	See justification table
Calculated decay rate	λ	6.93E-10	days ⁻¹	See justification table
Width of plume in aquifer at source (perpendicular to flow)	S_z	8.00E+02	m	See justification table
Plume thickness at source	S_y	2.50E+01	m	See justification table
Saturated aquifer thickness	d_a	3.00E+01	m	See justification table
Bulk density of aquifer materials	ρ	2.17E+00	g/cm ³	See justification table
Effective porosity of aquifer	n	1.00E-01	fraction	See justification table
Hydraulic gradient	I	1.20E-02	fraction	See justification table
Hydraulic conductivity of aquifer	K	4.77E-01	m/d	See justification table
Distance to compliance point	x	1.39E+02	m	See justification table
Distance (lateral) to compliance point perpendicular to flow direction	z	0.00E+00	m	See justification table
Distance (depth) to compliance point perpendicular to flow direction	y	0.00E+00	m	See justification table
Time since pollutant entered groundwater	t	1.00E+100	days	time variant options only
Parameters values determined from options				
Partition coefficient	K_d	3.60E+01	l/kg	see options
Longitudinal dispersivity	α_x	1.39E+01	m	see options
Transverse dispersivity	α_z	1.39E+00	m	see options
Vertical dispersivity	α_y	1.39E-01	m	see options

Calculated Parameters

Groundwater flow velocity	V	5.72E-02	m/d
Retardation factor	R_f	7.82E+02	fraction
Decay rate used	λ	6.93E-10	d ⁻¹
Rate of contaminant flow due to retardation	u	7.32E-05	m/d
Contaminant concentration at distance x, assuming one-way vertical dispersion	C_{ED}	4.00E-02	mg/l
Attenuation factor (one way vertical dispersion, CO/CED)	AF	1.00E+00	

Remedial Targets

Remedial Target	1.00E-02	mg/l	For comparison with measured groundwater concentration.
Ogata Banks			
Distance to compliance point	139	m	
Concentration of contaminant at compliance point after	C_{ED}/C_0 4.00E-02	mg/l	Ogata Banks
	1.0E+100	days	

Care should be used when calculating remedial targets using the time variant options as this may result in an overestimate of the remedial target. The recommended value for time when calculating the remedial target is 9.9E+99.

Select Method for deriving Partition Co-efficient (using pull down menu)

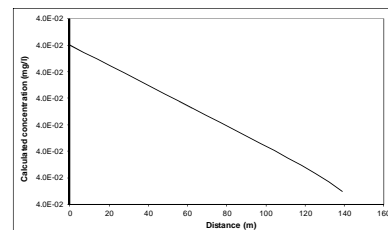
User specified value for partition coefficient

Entry if specify partition coefficient (option)		
Soil water partition coefficient	K_d	3.60E+01 l/kg
Entry for non-polar organic chemicals (option)		
Fraction of organic carbon in aquifer	f_{oc}	fraction
Organic carbon partition coefficient	K_{oc}	l/kg
Entry for ionic organic chemicals (option)		
Sorption coefficient for related species	K_{ow}	l/kg
Sorption coefficient for ionised species	K_{ow}	l/kg
pH value	pH	fraction
acid dissociation constant	pKa	fraction
Fraction of organic carbon in aquifer	f_{oc}	fraction
Soil water partition coefficient	K_d	3.60E+01 l/kg

Define dispersivity (click brown cell and use pull down list)

Dispersivities 10%, 1%, 0.1% of pathway length

Longitudinal dispersivity	α_x	Enter value	Calc value	α_x & Eckstein	m
Transverse dispersivity	α_z	1.00E+00	1.39E+01	5.23E+00	m
Vertical dispersivity	α_y	0.00E+00	1.39E+00	5.23E-01	m
Vertical dispersivity	α_y	0.00E+00	1.39E-01	5.23E-02	m
Note values of dispersivity must be > 0					
For calculated value, assumes $\alpha_x = 0.1 * x$, $\alpha_z = 0.01 * x$, $\alpha_y = 0.001 * x$					
α_x & Eckstein (1995) report $\alpha_x = 0.83(\log_{10} x)^{0.414}$; $\alpha_z = \alpha_x/10$, $\alpha_y = \alpha_x/100$ are assumed					



Note graph assumes plume disperses vertically in one direction only. An alternative solution assuming the centre of the plume is located at the mid-depth of the aquifer is presented in the calculation sheets.

Note

This sheet calculates the Level 3 remedial target for groundwater, based on the distance to the receptor or compliance located down hydraulic gradient of the source Three solution methods are included, the preferred option is Ogata Banks.

By setting a long travel time it will give the steady state solution, which should be used to calculate remedial targets.

The measured groundwater concentration should be compared with the Level 3 remedial target to determine the need for further action.

Note if contaminant is not subject to first order degradation, then set half life as 9.0E+99.

This worksheet should be used if pollutant transport and degradation is best described by a first order reaction. If degradation is best described by an electron limited degradation such as oxidation by O₂, NO₃, SO₄ etc than an alternative solution should be used

Calculated concentrations for distance-concentration graph

Distance	Concentration
0	4.0E-02
7.0	4.01E-02
13.9	4.01E-02
20.9	4.01E-02
27.8	4.01E-02
34.8	4.01E-02
41.7	4.01E-02
48.7	4.01E-02
55.6	4.01E-02
62.6	4.01E-02
69.5	4.01E-02
76.5	4.01E-02
83.4	4.01E-02
90.4	4.01E-02
97.3	4.01E-02
104.3	4.01E-02
111.2	4.01E-02
118.2	4.01E-02
125.1	4.01E-02
132.1	4.00E-02
139.0	4.00E-02

Appendix E. Gas Monitoring Results

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Borehole Number	Date of monitoring	Baro. Pressure	Relative Pressure	Depth of Installation	Response Zone	Install Ref	Diameter	CH ₄	CO ₂	O ₂	H ₂ S	CO	Gas Flow Rate	Water Level	GSV CH4	GSV CO2
		mbar	mbar	mbgl				peak	peak	Min	peak	peak	peak			
								(% vol)	(% vol)	(% v)	(ppm)	(ppm)	(l/h)			
BH03	11/07/2019			4.5	Made Ground											
	21/07/2019	995	0	4.5		1	50	10.7	1.6	10	0	80	0	DRY	0	0
	31/07/2019	1000	0	4.5		1	50	28.7	3.8	5.3	0	63	0	4.25	0	0
	06/08/2019	988	0	4.5		1	50	84.7	4.6	0	0	10	0	4.42	0	0
	20/08/2019			4.5			50	58.7	5.9	0.3	2	2000	2.1	4.48	1.2327	0.1239
	29/08/2019	1000	0.02	4.5		1	50	68.5	12.3	0.3	5	118	0.1	4.4	0.0685	0.0123
	06/09/2019	1003	0.17	4.5		1	50	75.3	17.7	0.7	6	24	0	4.46	0	0
	1			4.5				86.2	8.4	1.3	1	0	11.7	4.16	10.0854	0.9828
	2			4.5				0.9	0.1	21.3	0	0	0.1	0.62	0.0009	0.0001
	3			4.5				1.2	0.1	17.8	0	8	0.2	0.66	0.0024	0.0002
	Max (Min O2)							86.2	17.7	0	6	2000	11.7	4.48	10.0854	2.0709
BH04	11/07/2019			12.5	Weathered Bedrock											
	21/07/2019			12.5												
	31/07/2019	995	0	12.5		1	50	0	0	20.6	0	0	0	5.48	0	0
	06/08/2019	984	0	12.5		1	50	0	1.2	18.8	0	0	0	5.42	0	0
	20/08/2019	1008	0.14	12.5		1	50	0	0.1	21.2	0	1	0.2	5.45	0	0.0002
	29/08/2019	1001	0.07	12.5		1	50	0	6.2	13.6	0	4	0.2	5.42	0	0.0124
	06/09/2019	1002	0.1	12.5		1	50	0	0.7	12.9	0	0	0.1	5.48	0	0.0007
	1			12.5				0	0.1	21.2	0	0	0	5.22	0	0
	2			12.5				0	8.9	9.6	0	1	0.2	5.1	0	0.0178
	3			12.5				0.1	8.5	16.7	0	1	0.2	5.04	0.0002	0.017
	Max (Min O2)							0.1	8.9	9.6	0	4	0.2	5.48	0.0144	1.2816
BH05	11/07/2019			12	Weathered Bedrock											
	21/07/2019			12												
	31/07/2019	995	0	12		1	50	0	0	20.4	0	0	5.1	3.79	0	0
	06/08/2019	984	0	12		1	50	0	0	20.3	0	0	0	5.42	0	0
	20/08/2019	1008	0.16	12		1	50	0	0.1	20.9	0	0	0.4	3.73	0	0.0004
	29/08/2019	1001	0.03	12		1	50	0	0.1	20.6	0	4	0.2	3.7	0	0.0002
	06/09/2019	1002	0.1	12		1	50	0	0.1	20.5	0	1	0.1	3.72	0	0.0001
	1			12				0	1	19.7	0	1	-2	3.48	0	-0.02
	2			12				0.1	1.8	20.3	0	1	-0.5	3.41	-0.0005	-0.009
	3			12				0.1	0.4	21.7	0	1	0.3	3.27	0.0003	0.0012
	Max (Min O2)							0.1	1.8	19.7	0	4	5.1	5.42	0.0051	0.0918
BH06	11/07/2019			21	Superficial Deposits											
	21/07/2019			21												
	31/07/2019	995	0	21		1	50	0	0.4	18.3	0	12	5.7	3.52	0	0.0228
	06/08/2019	985	0	21		1	50	0	0.5	17.5	0	10	6.2	3.47	0	0.031
	20/08/2019	1008	0.09	21		1	50	0.1	0.9	16.6	0	20	0.1	8.4	0.0001	0.0009
	29/08/2019	1001	0.02	21		1	50	0.1	1	16.6	0	31	2.8	3.47	0.0028	0.028
	06/09/2019	1002	0.16	21		1	50	0.1	0.8	18.4	0	27	0	3.31	0	0
	1			21				0	3.4	12.1	2	99	1	3.22	0	0.034
	2			21				Gas Monitoring not needed.						3.13		
	3			21				Gas Monitoring not needed.						3.06		
	Max (Min O2)							0.1	3.4	12.1	2	99	6.2	8.4	0.0062	0

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BH07	11/07/2019			15.5	Superficial Deposits												
	21/07/2019			15.5													
	31/07/2019	996	0	15.5		1	50	0	0.2	13.6	0	63	0	6.45	0	0	
	06/08/2019	985	0	15.5		1	50	0	0.2	12.5	0	53	0	6.44	0	0	
	20/08/2019	1008	0.05	15.5		1	50	0.2	0.1	14.8	0	59	0.4	6.4	0.0008	0.0004	
	29/08/2019	1001	0.02	15.5		1	50	0.2	0.1	13.5	0	78	0.1	6.4	0.0002	0.0001	
	06/09/2019	1002	0.12	15.5		1	50	0	0	20.2	0	2	0.1	6.46	0	0	
	1			15.5					0.9	0.1	12.4	0	5	0.1	5.15	0.0009	0.0001
	2			15.5					0.2	0.1	20.6	0	1	0.1	5.08	0.0002	0.0001
	3			15.5					0.1	0.1	21.4	0	1	0.3	5.03	0.0003	0.0003
	Max (Min O2)								0.9	0.2	12.4	0	78	0.4	6.46	0.0036	0.0008
BH08a	11/07/2019	1005	0.02	28.2	Bedrock	1	50	0.2	0.3	19.8	0	4	0.2	3.55	0.0004	0.0006	
	21/07/2019	993	0	28.2		1	50	0	0.3	20.4	25	240	1.8	3.65	0	0.0054	
	31/07/2019	993	0	28.2		1	50	0	0.4	20	0	67	3.5	3.64	0	0.014	
	06/08/2019	987	0	28.2		1	50	0	0.5	19.8	0	32	2.5	3.65	0	0.0125	
	20/08/2019	1005	0.03	28.2		1	50	0.1	0.6	19.7	1	0	2.7	3.6	0.0027	0.0162	
	29/08/2019	1000	0.28	28.2		1	50	0	0.7	18.8	1	0	1.6	3.79	0	0.0112	
	06/09/2019	1003	0.05	28.2		1	50	0.3	0.8	18.9	0	0	0.3	3.65	0.0009	0.0024	
	1			28.2					0	2.1	18.9	0	0	0.1	3.1	0	0.0021
	2			28.2				Gas Monitoring not needed.						2.06			
	3			28.2				Gas Monitoring not needed.						3.01			
	Max (Min O2)								0.3	2.1	18.8	25	240	3.5		0.0105	0.0735
BH09	11/07/2019	994	0.1	27	Weathered Bedrock	1	50	4.4	2.1	11.5	1	66	0.1	9.28	0.0044	0.0021	
	21/07/2019	994	0	27		1	50	0	0.3	19	0	13	0.4	9.25	0	0.0012	
	31/07/2019	993	0	27		1	50	1.2	0.1	16.6	0	10	0.8	9.25	0.0096	0.0008	
	06/08/2019	987	0	27		1	50	2	0.4	13.7	0	36	1.3	9.21	0.026	0.0052	
	20/08/2019	1005	0.03	27		1	50	1.1	0.3	17.2	1	119	2.8	9.22	0.0308	0.0084	
	29/08/2019	1000	0.03	27		1	50	2.7	0.8	13.1	2	293	3	9.17	0.081	0.024	
	06/09/2019	1003	5.27	27		1	50	3.4	1.1	13.4	1	446	0.8	8.21	0.0272	0.0088	
	1			27					7.1	0.1	10.3	5	21	14.4	8.91	1.0224	0.0144
	2			27					2.2	0.2	18.8	0	4	0.2	8.85	0.0044	0.0004
	3			27					2.8	0.1	19.7	0	4	0.2	8.83	0.0056	0.0002
	Max (Min O2)								7.1	2.1	10.3	5	446	14.4		1.0224	0.3024
BH10	11/07/2019	994	0.4	13.5	Superficial deposits	1	50	0	0.1	19.9	0	18	0.0	5.63	0	0	
	21/07/2019	995	0	13.5		1	50	0	0.1	20.7	0	0	0	5.8	0	0	
	31/07/2019	995	0	13.5		1	50	0	0	20.3	0	0	0	5.77	0	0	
	06/08/2019	988	0	13.5		1	50	0	0.2	20.5	0	0	0	5.73	0	0	
	20/08/2019	1005	0	13.5		1	50	0.1	0.1	19.5	0	0	0.1	8.69	0.0001	0.0001	
	29/08/2019	1000	0.05	13.5		1	50	0	0.2	18.5	1	4	0.2	5.67	0	0.0004	
	06/09/2019	1003	0.02	13.5		1	50	0	0.1	20.6	0	0	0.1	7.7	0	0.0001	
	1			13.5					0	2.5	17.3	0	0	0.6	5.16	0	0.015
	2			13.5					0.1	2.8	19	0	0	-1.1	5.01	-0.0011	-0.0308
	3			13.5					0	2.1	19.2	0	0	-3.1	4.89	0	-0.0651
	Max (Min O2)								0.1	2.8	17.3	1	18	0.6		0.0006	0.0168

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BH11	11/07/2019	995	0.03	14	Weathered Bedrock	1	50	0.1	0.1	20.6	0	1	0.3	4.59	0.0003	0.0003
	21/07/2019	995	0	14		1	50	0	0.1	20.9	0	0	0	4.6	0	0
	31/07/2019	993	0	14		1	50	0	0.2	20.4	0	12	0	4.33	0	0
	06/08/2019	988	3	14		1	50	0	0	20.2	0	0	0	4.88	0	0
	20/08/2019	1005	0.002	14		1	50	0.1	0.1	20.5	0	1	0.1	4.92	0.0001	0.0001
	29/08/2019	1001	0.02	14		1	50	0	0.1	19.6	0	2	0.2	4.87	0	0.0002
	06/09/2019	1004	0.03	14		1	50	0	0.2	20.8	0	0	0	4.9	0	0
	1			14				0	1.4	20.4	0	0	0.2		0	0.0028
	2			14				Couldn't get access as Mr Shacklock revoked access.								
	3			14				0.1	0.6	21.3	0	1	0.2		0.0002	0.0012
	4							0.3	0.4	21	0	4	0.3	4.13	0.0009	0.0012
	Max (Min O2)							0.3	1.4	19.6	0	12	0.3		0.0009	0.0042

BH12	11/07/2019			5	Superficial Deposits											
	21/07/2019			5												
	31/07/2019			5												
	06/08/2019	987	0	5		1	50	0	0	20.2	0	41	0	1.19	0	0
	20/08/2019	1006	0.05	5		1	50	0.1	0.1	20.9	0	3	0.1	0.27	0.0001	0.0001
	29/08/2019	1001	0.05	5		1	50	0	0	19.9	1	6	0.2	1.26	0	0
	06/09/2019	1004	0.07	5		1	50	0	0.1	20.9	0	1	0	1.4	0	0
	1			5				0	0.1	21.3	0	0		0.62	0	0
	2			5				Couldn't get access as Mr Shacklock revoked access.								
	3			5				0.1	0.2	21.5	0	1	0.2	0.62	0.0002	0.0004
	4			5				0.2	0.1	21	0	4			0	0
	Max (Min O2)							0.2	0.2	19.9	1	41	0.2		0.0004	0.0004

BH16	11/07/2019			12	Superficial Deposits											
	21/07/2019			12												
	31/07/2019			12												
	06/08/2019			12												
	20/08/2019	1008	0.1	12		1	50	0.1	0	20.4	0	18	0.5	8.68	0.0005	0
	29/08/2019	1000	0.03	12		1	50	0.1	0	20.5	0	209	0.1	7.7	0.0001	0
	06/09/2019	996	0.03	12		1	50	0.1	0	20.8	0	262	0.1	7.77	0.0001	0
	1			12				0	0.1	21	0	8	0.2	6.99	0	0.0002
	2			12				0.1	0.1	21.4	0	1	0.1	6.92	0.0001	0.0001
	3			12				0.1	0.1	21.4	0	0	0.1	6.77	0.0001	0.0001
	Max (Min O2)							0.1	0.1	20.4	0	262	0.5		0.0005	0.0005

Water sample taken at 11.10m

BH18	11/07/2019			12	Weathered Bedrock											
	21/07/2019	993	0	12		1	50	0	0	15.7	0	278	0	3.48	0	0
	31/07/2019	996	0	12		1	50	0	0	20.6	0	0	0	3.50	0	0
	06/08/2019	987	0	12		1	50	0	0	14.2	0	122	0	3.53	0	0
	20/08/2019	1006	0.03	12		1	50	0.1	0	21	0	1	0.1	3.5	0.0001	0
	29/08/2019	1000	0.33	12		1	50	0	0.1	16.7	0	17	0.1	3.5	0	0.0001
	06/09/2019	996	0.09	12		1	50	0	0.2	18	0	0	0	3.55	0	0
	1			12				0.6	1	19.6	0	0	0	2.24	0	0
	2			12				0.1	1.6	19.3	0	0	0.2	1.96	0.0002	0.0032
	3			12				0.2	1.6	19.3	0	1	3.3	1.55	0.0066	0.0528
	Max (Min O2)							0.6	1.6	14.2	0	278	3.3		0.0198	0.0528

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BH20	11/07/2019			15	Weathered Bedrock											
	21/07/2019	993	0	15		1	50	0	0	18	0	59	0	12.8	0	0
	31/07/2019	995	0	15		1	50	0	0	20.6	0	0	0	12.2	0	0
	06/08/2019	988	0	15		1	50	0	0	20.4	0	0	0	12.96	0	0
	20/08/2019	1006	0.07	15		1	50	0.1	0	21.1	0	1	0.1	12.87	0.0001	0
	29/08/2019	1001	0.09	15		1	50	0	0	18	0	19	0.2	12.23	0	0
	06/09/2019	996	0.09	15		1	50	0	0.1	21	0	0	0.1	12.46	0	0.0001
	1			15				0	2.2	19.2	0	0	0	2.24	0	0
	2			15				0.1	3.1	18.9	0	0	0.2	1.96	0.0002	0.0062
	3			15				0.1	2.9	18.8	0	1	3.3	1.55	0.0033	0.0957
	Max (Min O2)							0.1	3.1	18	0	59	3.3		0.0033	0.1023

BH21	11/07/2019			5	Superficial Deposits											
	21/07/2019			5												
	31/07/2019			5												
	06/08/2019			5												
	20/08/2019	1008	0.02	5		1	50	0.1	0	18.7	1	125	1.6	1.83	0.0016	0
	29/08/2019	1001	0	5		1	50	0	0	18	1	366	0	1.99	0	0
	06/09/2019	996	0.05	5		1	50	0.1	0	17.9	1	147	0.5	1.98	0.0005	0
	1			5				0.6	1.3	15.9	0	4	-2.8	1.15	-0.0168	-0.0364
	2			5				3.3	0.1	16.8	0	7	20.4	1.03	0.6732	0.0204
	3			5				0.1	0.1	20	0	2	0.2	1.35	0.0002	0.0002
	Max (Min O2)							3.3	1.3	15.9	1	366	20.4	1.99	0.6732	0.2652

Water sample taken at 4.40m

BH22A	11/07/2019			29	Bedrock											
	21/07/2019			29												
	31/07/2019			29												
	06/08/2019			29												
	20/08/2019			29		1	50							0		
	29/08/2019			29		1	50							0		
	06/09/2019			29		1	50							0		
	1			29				Artesian Water so couldn't do gas analysis.								
	2			29				Artesian Water so couldn't do gas analysis.								
	3			29				Artesian Water so couldn't do gas analysis.								
	Max (Min O2)															

Low flow of water from top of standpipe.

BH24	11/07/2019			8	Superficial Deposits											
	21/07/2019	1001	0	8		1	50	0	1.8	7	0	114	0	4.05	0	0
	31/07/2019	1003	0	8		1	50	0	4.2	6.5	0	10	0	4.06	0	0
	06/08/2019	990	0	8		1	50	0	5.5	5.1	0	0	0	4.13	0	0
	20/08/2019	1008	0.05	8		1	50	0.1	7.4	4.4	0	3	0	4.1	0	0
	29/08/2019	1001	0.09	8		1	50	0.1	7.8	3.9	0	3	0	4.12	0	0
	06/09/2019	997	0.09	8		1	50	0.1	7	4	0	1	0	4.06	0	0
	1			8				0	8.1	6.8	0	9	3.8	3.28	0	0.3078
	2			8				0	0.6	21.2	0	0	0.2	3.11	0	0.0012
	3			8				0.1	1	21.2	0	1	0.2	3.01	0.0002	0.002
	Max (Min O2)							0.1	8.1	3.9	0	114	3.8		0.0038	0.3078

Gas and Groundwater Monitoring Results
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BH25	11/07/2019	1002	0	17	Superficial Deposits	1	50	0.1	0	19.1	1	197	0.3	7.41	0.0033	0
	21/07/2019	998	0	17		1	50	0	0	20.2	0	36	0	9.28	0	0
	31/07/2019	1002	0	17		1	50	0	0	18.8	0	26	0	8.62	0	0
	06/08/2019	990	0	17		1	50	0	0	14.2	0	10	0	9.03	0	0
	20/08/2019	1006	0	17		1	50	0.1	0	17.3	0	0	0	9.03	0	0
	29/08/2019	1000	0.02	17		1	50	0	0	15.2	0	0	0	8.94	0	0
	06/09/2019	997	0.02	17		1	50	0	0	13.8	0	0	0	9.03	0	0
	1			17				2.8	0.9	19.9	12	34	0	7.18	0	0
	2			17				5	0.3	18	1	10	-3.7	7.06	-0.185	-0.0111
	3			17				4.1	0.1	18.2	0	11	0.3	7.02	0.0123	0.0003
	Max (Min O2)							5	0.9	13.8	12	197	0.3		0.015	0.0027
BH26	11/07/2019			5	Superficial Deposits											
	21/07/2019			5												
	31/07/2019			5												
	06/08/2019	984	0	5		1	50	0	0	19.6	0	98	0	4.75	0	0
	20/08/2019	1008	0.14	5		1	50	0	0	19.7	1	169	0.1	4.84	0	0
	29/08/2019	1000	0.1	5		1	50	0.3	0	11.1	1	295	0.3	4.94	0.0009	0
	06/09/2019	997	0.1	5		1	50	0.3	0	15.5	1	185	0.1	4.87	0.0003	0
	1			5				0.9	0.1	8	0	11	0.1	4.76	0.0009	0.0001
	2			5				0.5	0.2	12	0	0	0.1	4.83	0.0005	0.0002
	3			5				0.5	0.2	11.9	0	1	0.3	5.01	0.0015	0.0006
	Max (Min O2)							0.9	0.2	8	1	295	0.3		0.0027	0.0006
BH27	11/07/2019			18	Weathered Bedrock											
	21/07/2019			18												
	31/07/2019	996	0	18		1	50	0	0	18.9	0	12	0	12.86	0	0
	06/08/2019	985	0	18		1	50	0	0.9	16.9	0	12	0	12.83	0	0
	20/08/2019	1008	0.1	18		1	50	0	0	20.1	0	140	0.1	12.99	0	0
	29/08/2019	1001	0.2	18		1	50	0	0	18.8	0	0	0.2	13.06	0	0
	06/09/2019	997	0.14	18		1	50	0	0.1	21.2	0	0	0.1	13.1	0	0.0001
	1			18												
	2			18				0.1	3.4	17.6	0	0	0.1	12.53	0.0001	0.0034
	3			18				0.1	1.5	19.5	0	1	0.1	12.48	0.0001	0.0015
	4			18				0.3	1.5	19	0	5	0.3	12.41	0.0009	0.0045
	Max (Min O2)							0.3	3.4	16.9	0	140	0.3	13.1	0.0009	0.0102